STORMWATER REPORT

Prepared For:

Ryder Development Corporation 668 Broad Street – Suite D Weymouth, Massachusetts 02189

Savanna Drive Subdivision Weymouth, Massachusetts

March 2022



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STORMWATER REPORT FOR SAVANNA DRIVE SUBDIVISION WEYMOUTH, MASSACHUSETTS

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SECTION 1

Narrative

NARRATIVE

STORMWATER REPORT SAVANNA DRIVE SUBDIVISION WEYMOUTH, MASSACHUSETTS

EXISTING CONDITIONS

The property is comprised of multiple parcels of land under common ownership, including a single-family home located at 65 Narragansett Avenue. With the exception of the 65 Narragansett Avenue lot, the majority of the subject property is wooded. Within the parcels are four paper streets, a municipal water main and a municipal sewer line. The property is generally bound by the Greenbush Line to the north, a salt marsh to the east, Commercial Street to the south, and Narragansett Avenue to the west. The property and abutting properties are zoned Residence (R-1).

The soil types on the property have been mapped by the USDA Natural Resources Conservation Service. The center area of the property is mapped as Rock outcrop-Hollis complex, well drained with a depth to water table of more than 80 inches. It is classified as Hydrologic Soil Group D.

The southwest area of the property is mapped as Hollis-Rock outcrop-Charlton complex, well drained with a depth to water table of more than 80 inches. The southeast area of the property is mapped as Charlton-Hollis-Rock outcrop complex, well drained with a depth to water table of more than 80 inches. These soil types are classified in Hydrologic Soils Groups D for its Hollis component. It should be noted that there is a significant presence of ledge outcrop on the site which confirms that the soils do not have a high capacity for stormwater acceptance.

The salt marsh area to the west is mapped as Ipswich mucky peat, very poorly drained with a depth to water table of about 0 inches. It is classified as Hydrologic Soil Group D.

There are no observed stormwater collection systems on the property. The majority of stormwater runoff flows overland from the property to the north and east, discharging to the salt marsh located in eastern the portion of the property. A relatively small portion of the subject property on the westerly side of the project site, including the 65 Narragansett Avenue lot flows in a westerly direction into the Narragansett Avenue storm drain system.

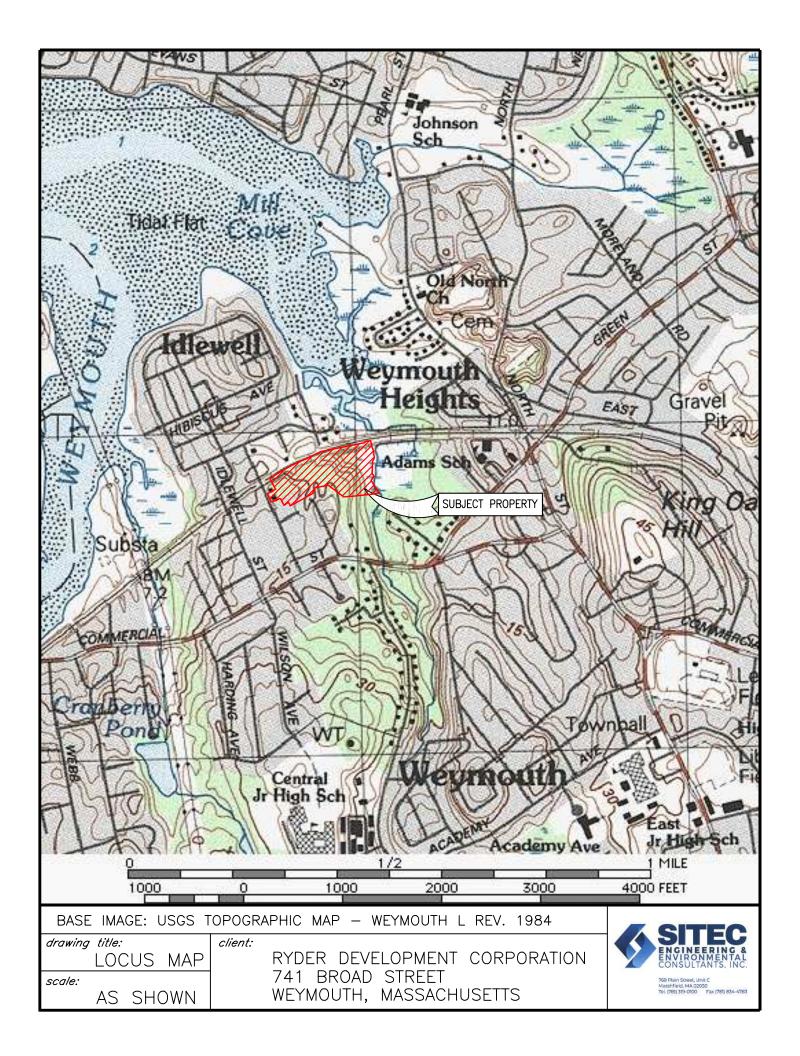
PROPOSED SITE CONDITIONS

The applicant proposes to subdivide the property into ten (10) single family home residential lots. Access and frontage for the lots will be created from the proposed Savanna Drive subdivision road. Savanna Drive will intersect with Narragansett Avenue and run through the 65 Narragansett Avenue lot to gain access to the lion's share of the project site. Municipal water will be provided from the existing Narragansett Avenue municipal main. Additionally, the proposed Savanna Drive water main will also be looped into the water main that crosses through the property. Sanitary sewer will be discharged to the existing municipal sewer main that crosses through the property. The remainder of utilities will brought in through Narragansett Avenue.

A subsurface stormwater collection system consisting of deep sump catchbasins, drain manholes, a stormwater treatment unit and a rip-rapped outlet is to be installed. The system will collect stormwater from the proposed roadway and its tributary drainage areas. Once collected, the stormwater will be discharged toward the tidally influenced salt marsh.

SECTION 2

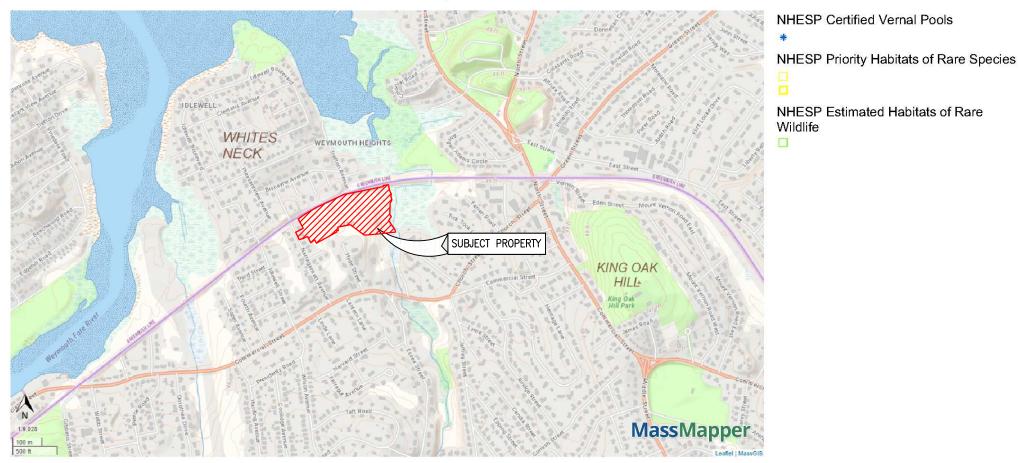
USGS Locus Map



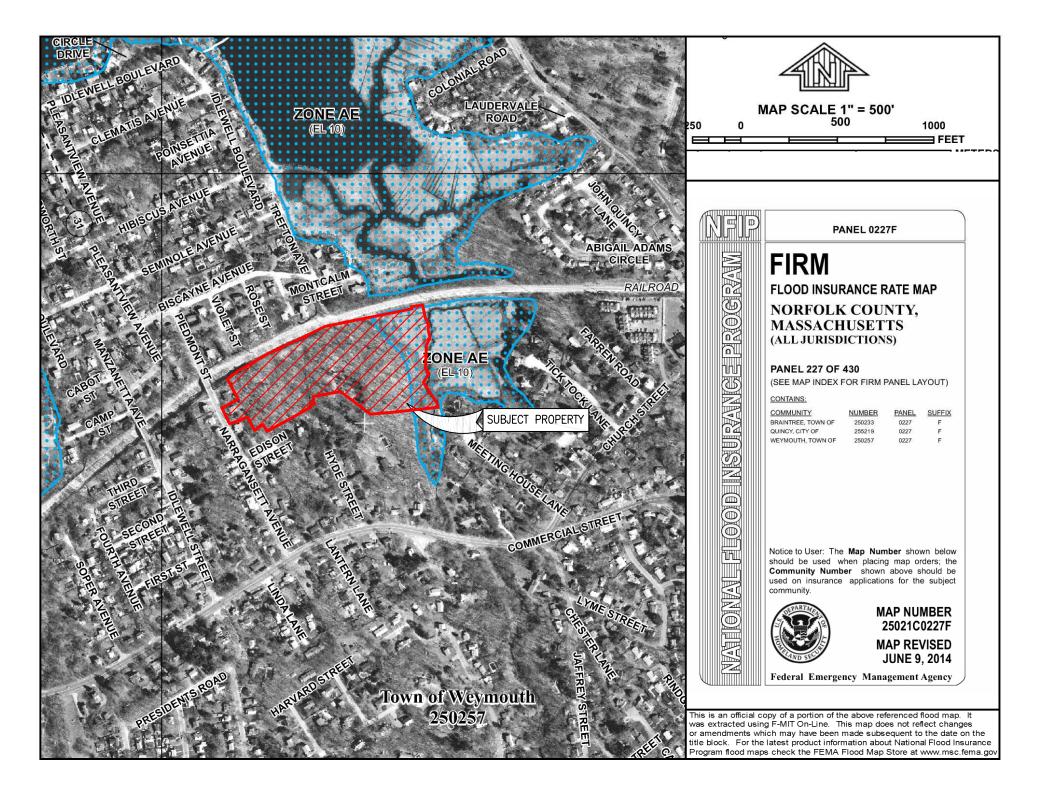
SECTION 3

Natural Heritage Map

NHESP Habitat Map - Savanna Drive Subdivision



SECTION 4 FEMA Flood Insurance Rate Map



SECTION 5 Soils Map



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey

MAP LEGEND				MAP INFORMATION		
Area of Interest (AOI)		😑 Spoil Area		The soil surveys that comprise your AOI were mapped at		
Area o	Area of Interest (AOI)		Stony Spot	1:25,000.		
Soils		0	Very Stony Spot	Warning: Soil Map may not be valid at this scale.		
	ap Unit Polygons	\$2	Wet Spot	Enlargement of maps beyond the scale of mapping can cause		
	ap Unit Lines	Å	Other	misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of		
-	ap Unit Points		Special Line Features	contrasting soils that could have been shown at a more detailed scale.		
Special Point Fe		Water Fea	atures	scale.		
 Blowor Borrow 		~	Streams and Canals	Please rely on the bar scale on each map sheet for map measurements.		
	nat	Transport	ation			
💥 Clay S		+++	Rails	Source of Map: Natural Resources Conservation Service Web Soil Survey URL:		
~	Depression	~	Interstate Highways	Coordinate System: Web Mercator (EPSG:3857)		
Gravel		~	US Routes	Maps from the Web Soil Survey are based on the Web Mercato		
0.0	ly Spot	\sim	🥪 Major Roads	projection, which preserves direction and shape but disto distance and area. A projection that preserves area, such		
🔇 Landfil	I	~	Local Roads	Albers equal-area conic projection, should be used if more		
🗎 🛛 Lava F	low	Backgrou	nd	accurate calculations of distance or area are required.		
📥 Marsh	or swamp	No.	Aerial Photography	This product is generated from the USDA-NRCS certified data a of the version date(s) listed below.		
🙊 Mine o	r Quarry					
Miscel	laneous Water			Soil Survey Area: Norfolk and Suffolk Counties, Massachuset Survey Area Data: Version 17, Sep 3, 2021		
O Perenr	nial Water			Soil map units are labeled (as space allows) for map scales		
🤝 🛛 Rock (Dutcrop			1:50,000 or larger.		
+ Saline	Spot			Date(s) aerial images were photographed: Aug 10, 2014—Oc 18, 2020		
sandy	Spot			The orthophoto or other base map on which the soil lines were		
Severe	ely Eroded Spot			compiled and digitized probably differs from the background		
Sinkho	le			imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.		
Slide of	r Slip					
g Sodic	Spot					



Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI			
65	Ipswich mucky peat, 0 to 2 percent slopes, very frequently flooded	1.2	12.0%			
103B	Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes	0.0	0.3%			
103C	Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes	3.7	38.7%			
104C	Hollis-Rock outcrop-Charlton complex, 0 to 15 percent slopes	0.5	5.0%			
105D	Rock outcrop-Hollis complex, 3 to 25 percent slopes	4.3	44.0%			
Totals for Area of Interest		9.7	100.0%			

Norfolk and Suffolk Counties, Massachusetts

65—Ipswich mucky peat, 0 to 2 percent slopes, very frequently flooded

Map Unit Setting

National map unit symbol: 2tyqj Elevation: 0 to 10 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 250 days Farmland classification: Not prime farmland

Map Unit Composition

Ipswich and similar soils: 90 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Ipswich

Setting

Landform: Tidal marshes Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear Parent material: Partially- decomposed herbaceous organic material

Typical profile

Oe - 0 to 42 inches: mucky peat Oa - 42 to 59 inches: muck

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water
(Ksat): Moderately low to very high (0.14 to 99.90 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: Very frequent
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Maximum salinity: Nonsaline to strongly saline (0.7 to 111.6 mmhos/cm)
Sodium adsorption ratio, maximum: 20.0
Available water supply, 0 to 60 inches: Very high (about 26.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8w Hydrologic Soil Group: A/D Ecological site: R144AY001CT - Tidal Salt Low Marsh mesic very frequently flooded, R144AY002CT - Tidal Salt High Marsh mesic very frequently flooded Hydric soil rating: Yes

Minor Components

Pawcatuck

Percent of map unit: 5 percent Landform: Tidal marshes Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear Ecological site: R144AY001CT - Tidal Salt Low Marsh mesic very frequently flooded, R144AY002CT - Tidal Salt High Marsh mesic very frequently flooded Hydric soil rating: Yes

Westbrook

Percent of map unit: 5 percent Landform: Tidal marshes Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear Ecological site: R144AY001CT - Tidal Salt Low Marsh mesic very frequently flooded, R144AY002CT - Tidal Salt High Marsh mesic very frequently flooded Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 17, Sep 3, 2021

Norfolk and Suffolk Counties, Massachusetts

103B—Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: vktd Elevation: 0 to 480 feet Mean annual precipitation: 32 to 54 inches Mean annual air temperature: 43 to 54 degrees F Frost-free period: 120 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Charlton and similar soils: 40 percent Hollis and similar soils: 25 percent Rock outcrop: 20 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Charlton

Setting

Landform: Hills Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Convex Parent material: Friable coarse-loamy ablation till derived from granite

Typical profile

H1 - 0 to 6 inches: fine sandy loam

H2 - 6 to 36 inches: fine sandy loam

H3 - 36 to 60 inches: fine sandy loam

Properties and qualities

Slope: 3 to 8 percent Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: More than 80 inches Drainage class: Well drained Runoff class: Low Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Available water supply, 0 to 60 inches: Moderate (about 7.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: A Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

Description of Hollis

Setting

Landform: Hills Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Convex Parent material: Shallow, friable loamy ablation till derived from igneous rock

Typical profile

H1 - 0 to 3 inches: fine sandy loam

- H2 3 to 14 inches: gravelly fine sandy loam
- H3 14 to 18 inches: unweathered bedrock

Properties and qualities

Slope: 3 to 8 percent
Surface area covered with cobbles, stones or boulders: 1.6 percent
Depth to restrictive feature: 10 to 20 inches to lithic bedrock
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 1.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: D Ecological site: F144AY033MA - Shallow Dry Till Uplands Hydric soil rating: No

Description of Rock Outcrop

Setting

Parent material: Igneous and metamorphic rock

Properties and qualities

Slope: 3 to 8 percent *Depth to restrictive feature:* 0 inches to lithic bedrock

Interpretive groups

Land capability classification (irrigated): None specified



Land capability classification (nonirrigated): 8s Hydric soil rating: Unranked

Minor Components

Canton

Percent of map unit: 7 percent Hydric soil rating: No

Chatfield

Percent of map unit: 5 percent Hydric soil rating: No

Scituate

Percent of map unit: 2 percent Hydric soil rating: No

Whitman

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 17, Sep 3, 2021

Norfolk and Suffolk Counties, Massachusetts

103C—Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2wzp1 Elevation: 0 to 1,390 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Charlton, extremely stony, and similar soils: 50 percent *Hollis, extremely stony, and similar soils:* 20 percent *Rock outcrop:* 10 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Charlton, Extremely Stony

Setting

Landform: Ridges, hills Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex, linear Across-slope shape: Convex Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material *A - 2 to 4 inches:* fine sandy loam *Bw - 4 to 27 inches:* gravelly fine sandy loam *C - 27 to 65 inches:* gravelly fine sandy loam

Properties and qualities

Slope: 8 to 15 percent
Surface area covered with cobbles, stones or boulders: 9.0 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water
(Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: B Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

Description of Hollis, Extremely Stony

Setting

Landform: Ridges, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex Across-slope shape: Linear, convex Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material *A - 2 to 7 inches:* gravelly fine sandy loam *Bw - 7 to 16 inches:* gravelly fine sandy loam *2R - 16 to 26 inches:* bedrock

Properties and qualities

Slope: 8 to 15 percent
Surface area covered with cobbles, stones or boulders: 9.0 percent
Depth to restrictive feature: 8 to 23 inches to lithic bedrock
Drainage class: Somewhat excessively drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: D Ecological site: F144AY033MA - Shallow Dry Till Uplands Hydric soil rating: No

Description of Rock Outcrop

Setting

Landform: Ridges, hills *Parent material:* Igneous and metamorphic rock

Typical profile

R - 0 to 79 inches: bedrock

Properties and qualities

Slope: 8 to 15 percent Depth to restrictive feature: 0 inches to lithic bedrock Runoff class: Very high Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr) Available water supply, 0 to 60 inches: Very low (about 0.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8 Hydrologic Soil Group: D Hydric soil rating: No

Minor Components

Woodbridge, extremely stony

Percent of map unit: 8 percent Landform: Ground moraines, hills, drumlins Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Canton, extremely stony

Percent of map unit: 5 percent Landform: Moraines, hills, ridges Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Chatfield, extremely stony

Percent of map unit: 5 percent Landform: Ridges, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex Across-slope shape: Linear, convex Hydric soil rating: No

Ridgebury, extremely stony

Percent of map unit: 2 percent Landform: Hills, drainageways, drumlins, depressions, ground moraines Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Head slope, base slope Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 17, Sep 3, 2021



Norfolk and Suffolk Counties, Massachusetts

104C—Hollis-Rock outcrop-Charlton complex, 0 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2w69p Elevation: 0 to 1,270 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Hollis, extremely stony, and similar soils: 35 percent
Charlton, extremely stony, and similar soils: 25 percent
Rock outcrop: 25 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hollis, Extremely Stony

Setting

Landform: Ridges, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex Across-slope shape: Linear, convex Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material *A - 2 to 7 inches:* gravelly fine sandy loam *Bw - 7 to 16 inches:* gravelly fine sandy loam *2R - 16 to 26 inches:* bedrock

Properties and qualities

Slope: 0 to 15 percent
Surface area covered with cobbles, stones or boulders: 9.0 percent
Depth to restrictive feature: 8 to 23 inches to lithic bedrock
Drainage class: Somewhat excessively drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: D Ecological site: F144AY033MA - Shallow Dry Till Uplands Hydric soil rating: No

Description of Charlton, Extremely Stony

Setting

Landform: Hills, ridges Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material *A - 2 to 4 inches:* fine sandy loam *Bw - 4 to 27 inches:* gravelly fine sandy loam *C - 27 to 65 inches:* gravelly fine sandy loam

Properties and qualities

Slope: 0 to 15 percent
Surface area covered with cobbles, stones or boulders: 9.0 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water
(Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: B Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

Description of Rock Outcrop

Setting

Landform: Ridges, hills *Parent material:* Igneous and metamorphic rock

Typical profile

R - 0 to 79 inches: bedrock

Properties and qualities

Slope: 0 to 15 percent Depth to restrictive feature: 0 inches to lithic bedrock Runoff class: Very high Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr) Available water supply, 0 to 60 inches: Very low (about 0.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8 Hydrologic Soil Group: D Hydric soil rating: No

Minor Components

Canton, extremely stony

Percent of map unit: 7 percent Landform: Moraines, hills, ridges Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Chatfield, extremely stony

Percent of map unit: 6 percent Landform: Ridges, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex Across-slope shape: Linear, convex Hydric soil rating: No

Montauk, extremely stony

Percent of map unit: 1 percent Landform: Hills, recessionial moraines, ground moraines, drumlins Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Scituate, extremely stony

Percent of map unit: 1 percent Landform: Ground moraines, hills, drumlins Landform position (two-dimensional): Summit, backslope, footslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex

Hydric soil rating: No

Data Source Information

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 17, Sep 3, 2021



Norfolk and Suffolk Counties, Massachusetts

105D—Rock outcrop-Hollis complex, 3 to 25 percent slopes

Map Unit Setting

National map unit symbol: vkxr Elevation: 0 to 620 feet Mean annual precipitation: 32 to 54 inches Mean annual air temperature: 43 to 54 degrees F Frost-free period: 120 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Rock outcrop: 65 percent Hollis and similar soils: 25 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Rock Outcrop

Setting

Parent material: Igneous and metamorphic rock

Properties and qualities

Slope: 15 to 25 percent *Depth to restrictive feature:* 0 inches to lithic bedrock

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s Hydric soil rating: Unranked

Description of Hollis

Setting

Landform: Hills Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Linear Across-slope shape: Convex Parent material: Shallow, friable loamy ablation till

Typical profile

H1 - 0 to 3 inches: fine sandy loam

H2 - 3 to 14 inches: gravelly fine sandy loam

H3 - 14 to 18 inches: unweathered bedrock

Properties and qualities

Slope: 3 to 25 percent Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 10 to 20 inches to lithic bedrock Drainage class: Well drained

Runoff class: High Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Available water supply, 0 to 60 inches: Very low (about 1.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: D Ecological site: F144AY033MA - Shallow Dry Till Uplands Hydric soil rating: No

Minor Components

Chatfield

Percent of map unit: 7 percent Hydric soil rating: No

Swansea

Percent of map unit: 2 percent Landform: Bogs Hydric soil rating: Yes

Whitman

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 17, Sep 3, 2021

SECTION 6

Wetland Delineation Memo

ECR Environmental Consulting & Restoration, LLC



WETLAND DELINEATION MEMO

TO: Alexander Trakimas @ SITEC Environmental, Inc.

FROM: Brad Holmes @ ECR, LLC

DATE: September 22, 2017

RE: off Edison Street/Hyde Street, Weymouth

Per your request, Environmental Consulting & Restoration, LLC (ECR) performed a review of the existing conditions at the properties located to the east of Edison Street and Hyde Street in Weymouth (the Site) on September 15, 2017. The purpose of the review was to locate the landward limit of a salt marsh associated with a tidal creek near the site. ECR did not perform a Bordering Vegetated Wetland (BVW) delineation at the site since the BVW was previously delineated by others. ECR placed Salt Marsh Flags #SM1 to #SM31 along the landward limit of the Salt Marsh where it transitions to a BVW. The delineation began along the northern side of the site nearest the train tracks and followed the marsh south until it dissipated and merged into a freshwater wetland.

Also review of the MassGIS wetlands database reveals the following:

- 1. The site <u>is not located</u> within Estimated/Priority Habitat for Rare Species according to the Massachusetts Natural Heritage & Endangered Species Program (MaNHESP).
- 2. The site does not contain Certified Vernal Pools according to MaNHESP.
- 3. The site <u>does abut</u> a U.S.G.S. mapped perennial stream. This stream is a tidal creek and would be measured at the Mean High Water line, which would designate the start of the 200 foot Riverfront Area.
- 4. The eastern portion of the site <u>is located</u> within an area mapped as Land Subject to Coastal Storm Flowage according to the FEMA Maps (Flood Zone AE).
- 5. The site is not located within an Area of Critical Environmental Concern (ACEC).

Upon review of this wetland delineation memo, please contact me at (617) 529 – 3792 or brad@ecrholmes.com with any questions or requests for additional information.

Thank you,



Brad Holmes, Professional Wetland Scientist #1464 Manager

SECTION 7 Stormwater Management System & Drainage Report



STORMWATER MANAGEMENT SYSTEM & DRAINAGE REPORT

Ryder Development Corporation 4-Lot Residential Subdivision Edison Street, Weymouth, MA

EXISTING CONDITIONS

The property is comprised of multiple parcels of land under common ownership, including a single-family home located at 65 Narragansett Avenue. With the exception of the 65 Narragansett Avenue lot, the majority of the subject property is wooded. Within the parcels are four paper streets, a municipal water main and a municipal sewer line. The property is generally bound by the Greenbush Line to the north, a salt marsh to the east, Commercial Street to the south, and Narragansett Avenue to the west. The property and abutting properties are zoned Residence (R-1).

The soil types on the property have been mapped by the USDA Natural Resources Conservation Service. The center area of the property is mapped as Rock outcrop-Hollis complex, well drained with a depth to water table of more than 80 inches. It is classified as Hydrologic Soil Group D.

The southwest area of the property is mapped as Hollis-Rock outcrop-Charlton complex, well drained with a depth to water table of more than 80 inches. The southeast area of the property is mapped as Charlton-Hollis-Rock outcrop complex, well drained with a depth to water table of more than 80 inches. These soil types are classified in Hydrologic Soils Groups D for its Hollis component. It should be noted that there is a significant presence of ledge outcrop on the site which confirms that the soils do not have a high capacity for stormwater acceptance.

The salt marsh area to the west is mapped as Ipswich mucky peat, very poorly drained with a depth to water table of about 0 inches. It is classified as Hydrologic Soil Group D.

There are no observed stormwater collection systems on the property. The majority of stormwater runoff flows overland from the property to the north and east, discharging to the salt marsh located in eastern the portion of the property. A relatively small portion of the subject property on the westerly side of the project site, including the 65 Narragansett Avenue lot flows in a westerly direction into the Narragansett Avenue storm drain system.



PROPOSED CONDITIONS DEP PERFORMANCE STANDARDS AND DESIGN CRITERIA

The DEP Stormwater Management Regulations include ten Stormwater Management Standards. The Standards were established to provide clear and consistent guidelines for stormwater management projects. The Standards address both water quantity and quality by establishing a level of required controls, which can presumptively be achieved through site planning processes, non-structural measures and the use of Best Management Practices (BMPs).

Each of the standards have been evaluated for their applicability to the proposed Definitive Subdivision as follows:

1. No new stormwater conveyances (outfalls/discharges) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

Stormwater runoff from proposed areas of roadway and driveway pavement shall be treated by the proposed stormwater controls. Surficial grading will convey stormwater runoff from paved areas, as well as other tributary areas including roof and yard runoff, into deep sump / hooded catch basins located in the roadway. Runoff will then flow through a network of piping into a stormwater treatment unit that will discharge runoff onto a rip rap lined velocity dissipating apron.

The volume of runoff to be treated for this project has been calculated as 1.0 inch of runoff times the total impervious area of the post-development project site. The term impervious area refers to impervious surfaces where 100% runoff would occur excluding roofs. The treatment calculation is attached to this report.

2. Stormwater management systems shall be designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates. This Standard may be waived for discharges to land subject to coastal storm flowage as defined in 310 CMR 10.04.

By definition - Land Subject to Coastal Storm Flowage means land subject to any inundation caused by coastal storms up to and including that caused by the 100-year storm, surge of record or storm of record, whichever is greater. The stormwater discharge from the project discharges to land subject to coastal storm flowage.



SITEC Environmental has prepared calculations for pre-development (existing) conditions and for post-development (proposed) conditions after the Definitive Subdivision has been fully constructed. The calculations have been performed for each of the 2, 10, and 100 year 24 hour storm events. One the following page is a summary table of existing and proposed flow rates discharging to land subject to coastal storm flowage (LSCSF).

		Storm Event		
		2- Year (3.4")	10- Year (4.7")	100- Year (7.0")
Flow Rates Discharging to LSCSF (cfs)	Existing Conditions	11.33	18.56	31.71
	Proposed Conditions	18.46	30.17	50.26

Stormwater Calculation Table for the 2, 10, and 100-Year Events

3. Loss of annual recharge to ground water should be minimized through the use of infiltration measures including environmentally sensitive site design, low impact development techniques, stormwater best management practices, and good operation and maintenance. At a minimum, the annual recharge from the post-development site shall approximate the annual recharge from pre-development conditions based on soil type. This Standard is met when the stormwater management system is designed to infiltrate the required recharge volume as determined in accordance with the Massachusetts Stormwater Handbook.

The majority of the site is mapped as D type soil. As such, the following required Volume to Recharge has been calculated based on the entire proposed impervious area for Hydrologic Soil Group D:

Hydrologic Group D Volume to Recharge =

0.10 inches of runoff (0.008 Feet) x Total Impervious Area in SF = CF



HSG-D (0.008 FT) x (46,227 SF of Impervious Area) = 370 CF

As noted in the Massachusetts Stormwater Handbook, Volume 1: Overview of Massachusetts Stormwater Standards, Chapter 1, pages 6 and 7, for sites comprised solely of C and D soils and bedrock at the land surface, proponents are required to infiltrate the required recharge volume only to the maximum extent practicable.

The vast majority of the subdivision project will be graded to promote overland flow from the residential lots to the salt marsh to the east of the project site. In our opinion, the infiltration provided from the overland flow will provide a high degree of infiltration.

In addition, if the soil conditions are appropriate, the applicant proposes to install leaching basins in the locations of the roadway catch basins. In our opinion, the leaching catch basins in conjunction with promoting overland flow using low-impact development surficial grading has provided recharge to groundwater to the maximum amount practicable.

- 4. Stormwater management systems shall be designed to remove 80% of the average annual post-construction load of Total Suspended Solids (TSS). This Standard is met when:
 - a. Suitable practices for source control and pollution prevention are identified in a long-term pollution prevention plan, and thereafter are implemented and maintained;
 - b. Structural stormwater best management practices are sized to capture the required water quality volume determined in accordance with the Massachusetts Stormwater Handbook; and,
 - c. Pretreatment is provided in accordance with the Massachusetts Stormwater Handbook.

BMPs that have been incorporated into stormwater management system and its operation include: pavement sweeping, deep sump and hooded catch basins and a proprietary stormwater treatment unit. DEP has developed a standard methodology for calculating TSS removal rates. This methodology assigns removal efficiencies to the various BMPs to be used on the project. This calculation is presented on a DEP "TSS Removal Calculation Worksheet", which is attached to this report. With the BMPs proposed for this project the calculated 80-percent TSS removal rate has been achieved.



5. For land uses with higher potential pollutant loads, source control and pollution prevention shall be implemented in accordance with the Massachusetts Stormwater Handbook to eliminate or reduce the discharge of stormwater runoff from such land uses to the maximum extent practicable. If through source control and/or pollution prevention all land uses with higher potential pollutant loads cannot be completely protected from exposure to rain, snow, snow melt, and stormwater runoff, the proponent shall use the specific structural stormwater BMPs determined by the Department to be suitable for such uses as provided in the Massachusetts Stormwater Handbook. Stormwater discharges from land uses with higher potential pollutant loads shall also comply with the requirements of the Massachusetts Clean Waters Act, M.G.L. c. 21, §§ 26-53 and the regulations promulgated thereunder at 314 CMR 3.00, 314 CMR 4.00 and 314 CMR 5.00.

There are no areas on the project site that may expose stormwater runoff to any higher potential pollutant loads. The structural BMPs that are proposed for control of the site's runoff and sediment demonstrate that the site will comply with this standard.

6. Stormwater discharges within the Zone II or Interim Wellhead Protection Area of a public water supply, and stormwater discharges near or to any other critical area, require the use of the specific source control and pollution prevention measures and the specific structural stormwater best management practices determined by the Department to be suitable for managing discharges to such areas, as provided in the Massachusetts Stormwater Handbook. A discharge is near a critical area if there is a strong likelihood of a significant impact occurring to said area, taking into account site-specific factors. Stormwater discharges to Outstanding Resource Waters and Special Resource Waters shall be removed and set back from the receiving water or wetland and receive the highest and best practical method of treatment. A "storm water discharge" as defined in 314 CMR 3.04(2)(a)1 or (b) to an Outstanding Resource Water or Special Resource Water shall comply with 314 CMR 3.00 and 314 CMR 4.00. Stormwater discharges to a Zone I or Zone A are prohibited unless essential to the operation of a public water supply.

Based on our research, the proposed Definitive Subdivision is not located within a Zone II or Interim Wellhead Protection Area of a public water supply or to any other critical area.



7. A redevelopment project is required to meet the following Stormwater Management Standards only to the maximum extent practicable: Standard 2, Standard 3, and the pretreatment and structural best management practice requirements of Standards 4, 5, and 6. Existing stormwater discharges shall comply with Standard 1 only to the maximum extent practicable. A redevelopment project shall also comply with all other requirements of the Stormwater Management Standards and improve existing conditions.

The proposed Definitive Subdivision is not a redevelopment project and the proposed stormwater management system has been designed to meet all performance standards.

8. A plan to control construction-related impacts including erosion, sedimentation and other pollutant sources during construction and land disturbance activities (construction period erosion, sedimentation, and pollution prevention plan) shall be developed and implemented.

During the construction phase, non-structural BMPs will be utilized to mitigate possible short term sedimentation. These temporary non-structural BMPs will include a silt barrier consisting of silt socks filled with compost which will be placed on the down gradient sides of roadways to prevent siltation to lower-lying areas. Haybale check dams or supplemental silt socks will also be placed around installed catch basins to prevent sediment from accumulating within the catch basins.

9. A long-term operation and maintenance plan shall be developed and implemented to ensure that stormwater management systems function as designed.

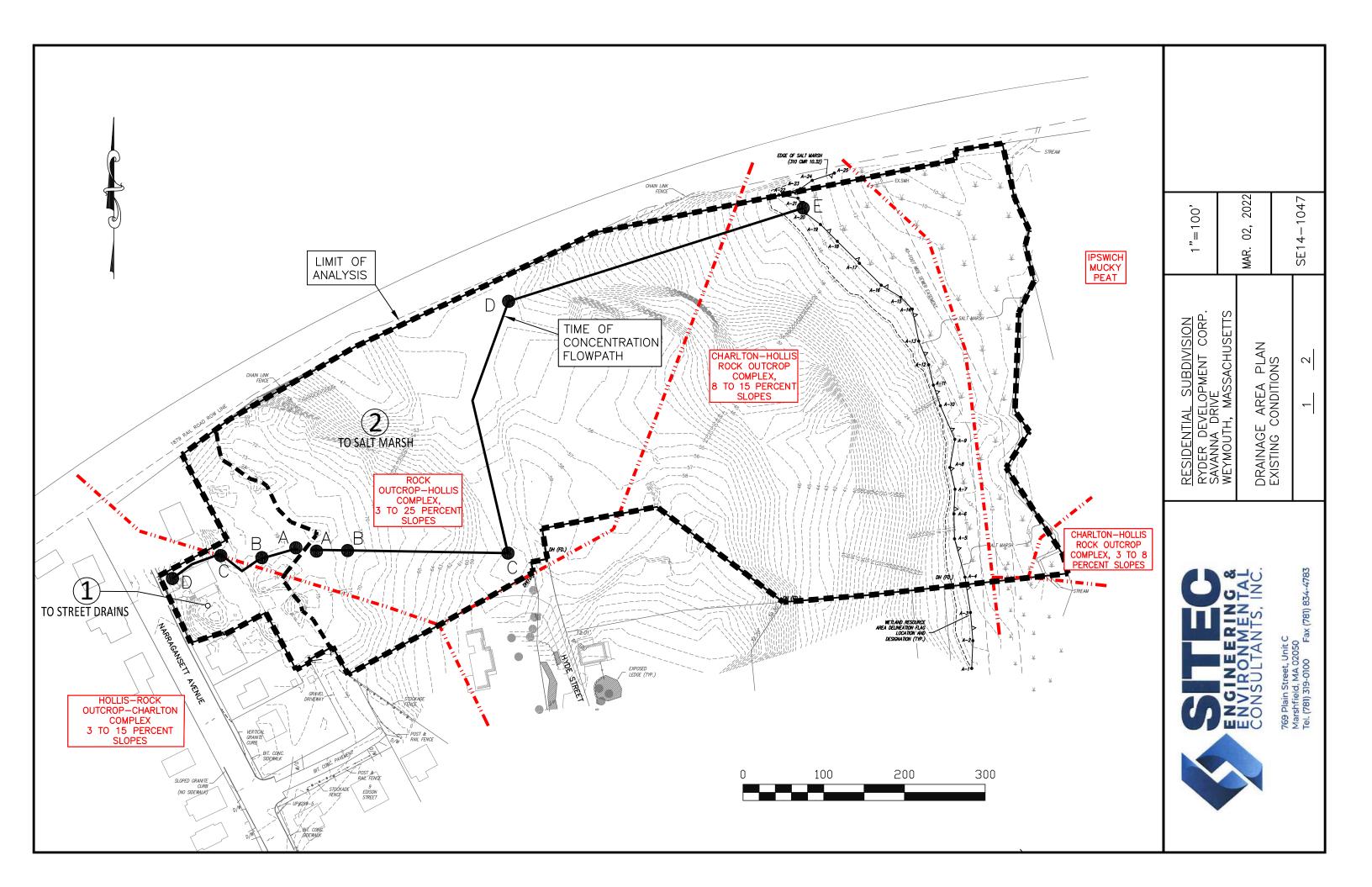
The Stormwater Management System Operation & Maintenance Plan for the project site is attached to this report.

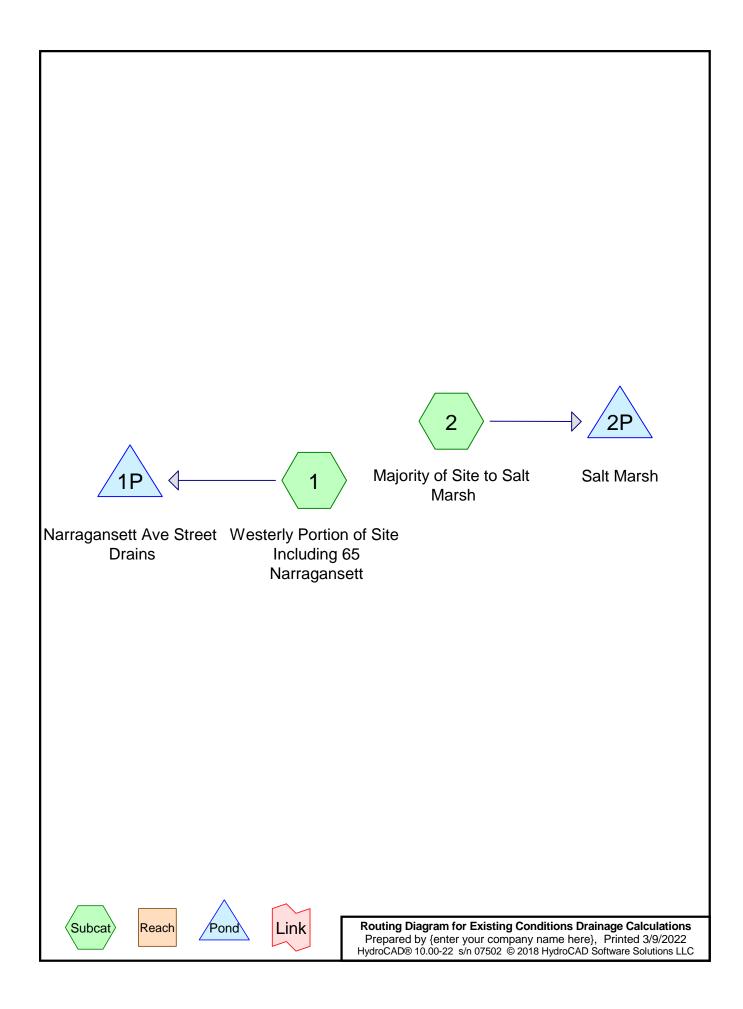
10. All illicit discharges to the stormwater management system are prohibited.

To the best of our professional knowledge and belief no illicit discharges exist on or are proposed on the site.

SECTION 8

Drainage Calculations & Drainage Area Plans





Summary for Subcatchment 1: Westerly Portion of Site Including 65 Narragansett

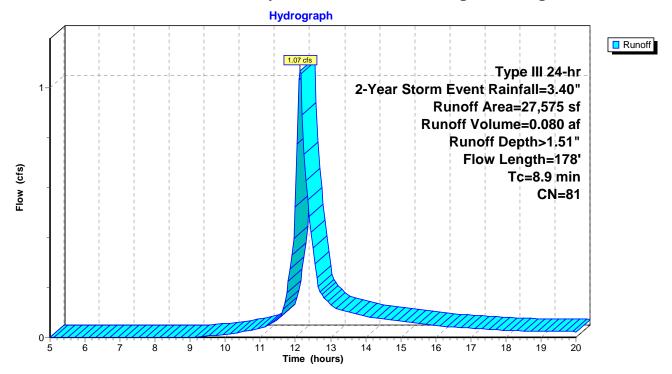
Runoff = 1.07 cfs @ 12.13 hrs, Volume= 0.080 af, Depth> 1.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Storm Event Rainfall=3.40"

	A	rea (sf)	CN E	Description			
*		1,382	98 F	Roofs/Deck	s, HSG D		
*		389	98 E	Driveway, F	ISG D		
		7,946	80 >	75% Gras	s cover, Go	ood, HSG D	
_		17,858	79 V	Voods, Fai	r, HSG D		
		27,575	81 V	Veighted A	verage		
		25,804	g	3.58% Pei	vious Area		
		1,771	6	5.42% Impe	ervious Area	a	
	_		<u>.</u>		•	— • • •	
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)						
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
_	8.3	(feet) 50	(ft/ft) 0.0070	(ft/sec) 0.10	(cfs)	Sheet Flow, AB	
		· /			(cfs)	Sheet Flow, AB Grass: Short n= 0.150 P2= 3.40"	
_		· /			(cfs)	Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC	
	8.3 0.4	50	0.0070 0.0200	0.10 2.28	(cfs)	Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC Unpaved Kv= 16.1 fps	
_	8.3	50	0.0070	0.10	(cfs)	Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC Unpaved Kv= 16.1 fps Shallow Concentrated Flow, CD	
_	8.3 0.4	50 60	0.0070 0.0200	0.10 2.28	(cfs)	Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC Unpaved Kv= 16.1 fps	

8.9 178 Total

Subcatchment 1: Westerly Portion of Site Including 65 Narragansett



Summary for Subcatchment 2: Majority of Site to Salt Marsh

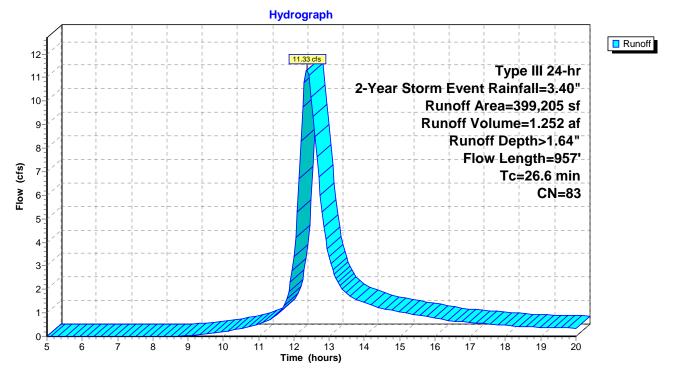
Runoff = 11.33 cfs @ 12.38 hrs, Volume= 1.252 af, Depth> 1.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Storm Event Rainfall=3.40"

_	A	rea (sf)	(sf) CN	Descriptior	า	
	3	24,786	786 79	Woods, Fa	ir, HSG D	
_	74,419 98 Water Surface, HSG D			Water Surf	ace, HSG D	
	3	99,205	205 83	Weighted /		
	3	24,786	786		rvious Area	
		74,419	419	18.64% lm	pervious Ar	ea
	т	L a sa ast la	a autho Olia		0	Description
	Tc (min)	Length	•			Description
-	(min)	(feet)	/ /	/ / /	(cfs)	
	11.5	50	50 0.02	21 0.07		Sheet Flow, AB
						Woods: Light underbrush n= 0.400 P2= 3.40"
	2.4	199	199 0.07	55 1.37		Shallow Concentrated Flow, BC
						Woodland Kv= 5.0 fps
	8.6	325	325 0.01	60 0.63		Shallow Concentrated Flow, CD
						Woodland Kv= 5.0 fps
	4.1	383	383 0.09	67 1.55		Shallow Concentrated Flow, DE
_						Woodland Kv= 5.0 fps
	~~ ~	057	0F7 T.L.			

26.6 957 Total

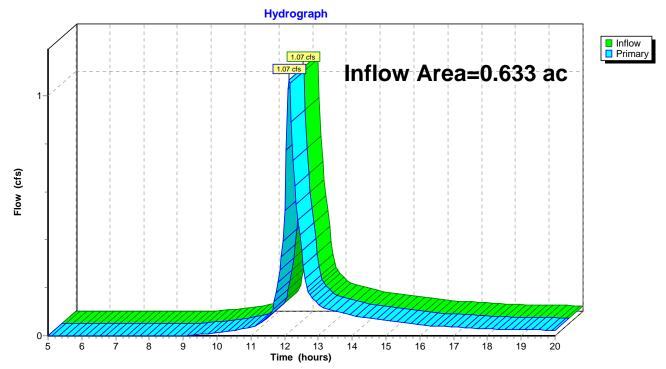
Subcatchment 2: Majority of Site to Salt Marsh



Summary for Pond 1P: Narragansett Ave Street Drains

Inflow Are	a =	0.633 ac,	6.42% Impervious, Inflow D	epth > 1.51"	for 2-Year Storm Event event
Inflow	=	1.07 cfs @	12.13 hrs, Volume=	0.080 af	
Primary	=	1.07 cfs @	12.13 hrs, Volume=	0.080 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

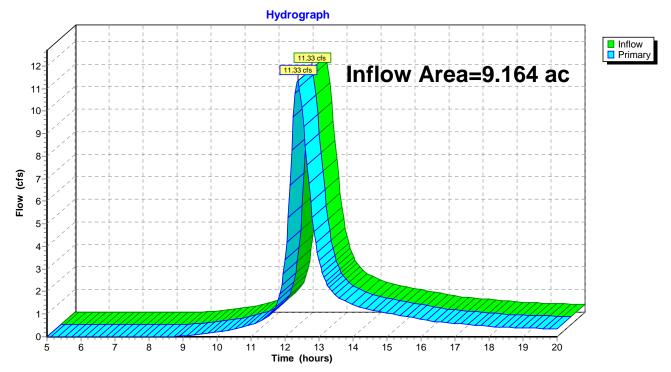


Pond 1P: Narragansett Ave Street Drains

Summary for Pond 2P: Salt Marsh

Inflow Are	a =	9.164 ac, 18.64% Impervious, Inflow Depth > 1.64" for 2-Year Storm Event event	
Inflow	=	11.33 cfs @ 12.38 hrs, Volume= 1.252 af	
Primary	=	11.33 cfs @ 12.38 hrs, Volume= 1.252 af, Atten= 0%, Lag= 0.0 min	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Pond 2P: Salt Marsh

Summary for Subcatchment 1: Westerly Portion of Site Including 65 Narragansett

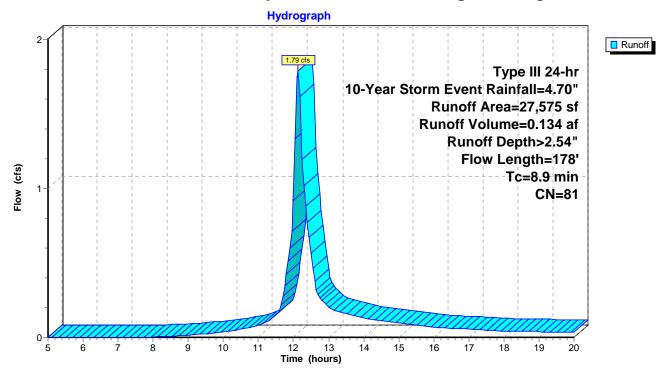
Runoff = 1.79 cfs @ 12.13 hrs, Volume= 0.134 af, Depth> 2.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Storm Event Rainfall=4.70"

_	A	rea (sf)	CN [Description		
*		1,382	98 F	Roofs/Deck	s, HSG D	
*		389	98 E	Driveway, H	ISG D	
		7,946	80 >	75% Gras	s cover, Go	ood, HSG D
_		17,858	79 V	Voods, Fai	ir, HSG D	
		27,575		Veighted A		
		25,804	-		rvious Area	
		1,771	6	5.42% Impe	ervious Area	а
	Тс	Longth	Class	Mala altri		Description
	10	Lendin	Slope	Velocity	Capacity	Description
	(min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_		•	•			Sheet Flow, AB
	(min)	(feet)	(ft/ft)	(ft/sec)		
_	(min)	(feet)	(ft/ft)	(ft/sec)		Sheet Flow, AB Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC
_	(min) 8.3 0.4	(feet) 50	(ft/ft) 0.0070 0.0200	(ft/sec) 0.10 2.28		Sheet Flow, AB Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC Unpaved Kv= 16.1 fps
	(min) 8.3	(feet) 50	(ft/ft) 0.0070	(ft/sec) 0.10		Sheet Flow, AB Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC Unpaved Kv= 16.1 fps Shallow Concentrated Flow, CD
_	(min) 8.3 0.4	(feet) 50 60	(ft/ft) 0.0070 0.0200	(ft/sec) 0.10 2.28		Sheet Flow, AB Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC Unpaved Kv= 16.1 fps

8.9 178 Total

Subcatchment 1: Westerly Portion of Site Including 65 Narragansett



Summary for Subcatchment 2: Majority of Site to Salt Marsh

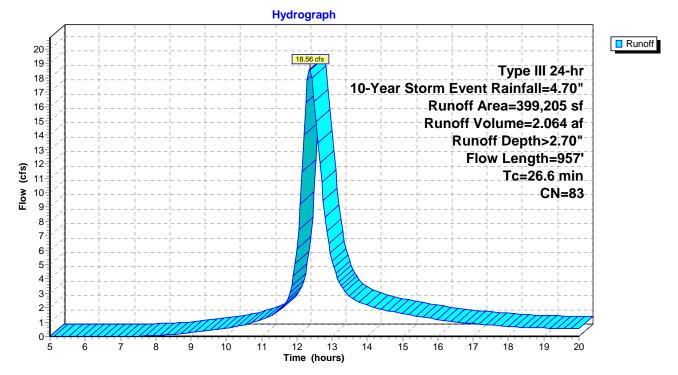
Runoff = 18.56 cfs @ 12.37 hrs, Volume= 2.064 af, Depth> 2.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Storm Event Rainfall=4.70"

A	rea (sf)	CN E	Description		
3	24,786	79 V	Voods, Fai	r, HSG D	
74,419 98 W		Vater Surfa	ace, HSG D		
399,205 8		83 V	Veighted A	verage	
3	24,786	8	1.36% Per	vious Area	
	74,419	1	8.64% Imp	pervious Ar	ea
-				o ''	
	•	•			Description
	(feet)	(11/11)		(CIS)	
11.5	50	0.0221	0.07		Sheet Flow, AB
					Woods: Light underbrush n= 0.400 P2= 3.40"
2.4	199	0.0755	1.37		Shallow Concentrated Flow, BC
		/			Woodland Kv= 5.0 fps
8.6	325	0.0160	0.63		Shallow Concentrated Flow, CD
	000	0.0007	4 55		Woodland Kv= 5.0 fps
4.1	383	0.0967	1.55		Shallow Concentrated Flow, DE
					Woodland Kv= 5.0 fps
	3	399,205 324,786 74,419 Tc Length (min) (feet) 11.5 50 2.4 199 8.6 325 4.1 383	324,786 79 V 74,419 98 V 399,205 83 V 324,786 8 74,419 1 324,786 8 74,419 1 Tc Length Slope (min) (feet) (ft/ft) 11.5 50 0.0221 2.4 199 0.0755 8.6 325 0.0160 4.1 383 0.0967	324,786 79 Woods, Fai 74,419 98 Water Surfa 399,205 83 Weighted A 324,786 81.36% Per 74,419 18.64% Imp 74,419 18.64% Imp Tc Length Slope Velocity (min) (feet) 11.5 50 2.4 199 0.0755 1.37 8.6 325 4.1 383 0.0967 1.55	324,786 79 Woods, Fair, HSG D 74,419 98 Water Surface, HSG D 399,205 83 Weighted Average 324,786 81.36% Pervious Area 324,786 81.36% Pervious Area 74,419 18.64% Impervious Area 11.5 50 0.0221 0.07 2.4 199 0.0755 1.37 8.6 325 0.0160 0.63 4.1 383 0.0967 1.55

26.6 957 Total

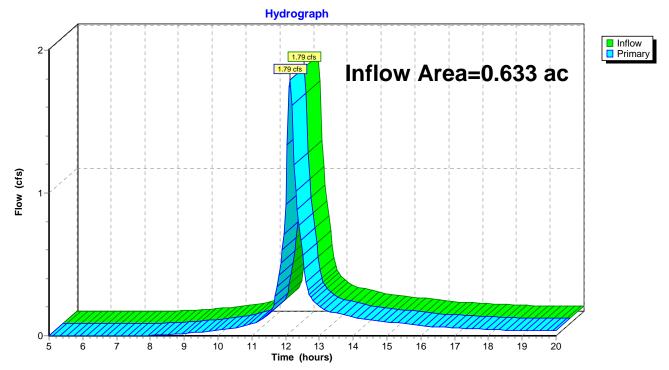
Subcatchment 2: Majority of Site to Salt Marsh



Summary for Pond 1P: Narragansett Ave Street Drains

Inflow Are	a =	0.633 ac,	6.42% Impervious, Inflow De	epth > 2.54"	for 10-Year Storm Event event
Inflow	=	1.79 cfs @	12.13 hrs, Volume=	0.134 af	
Primary	=	1.79 cfs @	12.13 hrs, Volume=	0.134 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

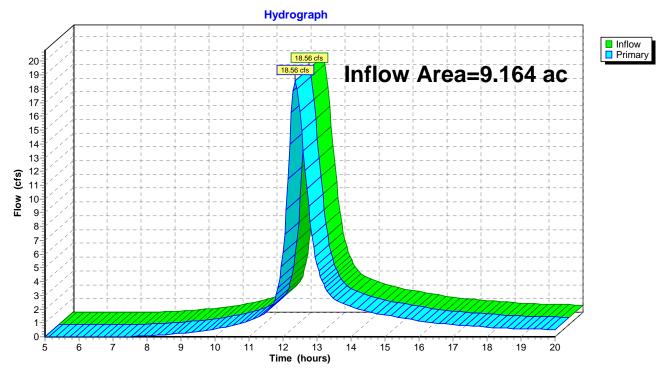


Pond 1P: Narragansett Ave Street Drains

Summary for Pond 2P: Salt Marsh

Inflow Are	a =	9.164 ac, 18.64% Impervious, Inflow Depth > 2.70" for 10-Year Storm Event event
Inflow	=	18.56 cfs @ 12.37 hrs, Volume= 2.064 af
Primary	=	18.56 cfs @ 12.37 hrs, Volume= 2.064 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Pond 2P: Salt Marsh

Summary for Subcatchment 1: Westerly Portion of Site Including 65 Narragansett

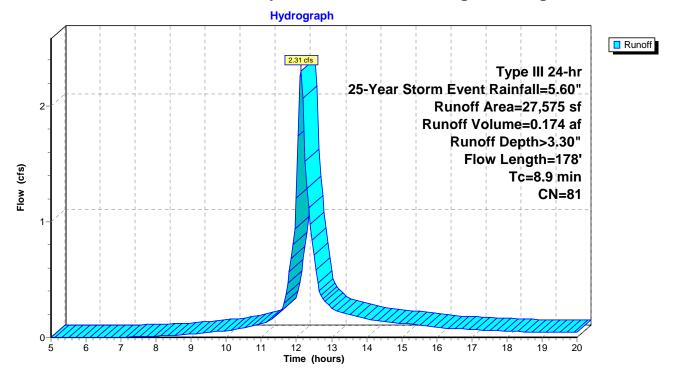
Runoff = 2.31 cfs @ 12.13 hrs, Volume= 0.174 af, Depth> 3.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Storm Event Rainfall=5.60"

_	A	rea (sf)	CN [Description		
*		1,382	98 F	Roofs/Deck	ks, HSG D	
*		389	98 E	Driveway, H	ISG D	
		7,946				ood, HSG D
		17,858	79 \	Voods, Fai	ir, HSG D	
		27,575		Veighted A	0	
		25,804	-		rvious Area	
		1,771	6	6.42% Impe	ervious Area	а
	Та	Longth	Clana	Valacity	Conceity	Description
	Tc (min)	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	Capacity (cfs)	
		•				Sheet Flow, AB
_	(min) 8.3	(feet) 50	(ft/ft) 0.0070	(ft/sec) 0.10		Sheet Flow, AB Grass: Short n= 0.150 P2= 3.40"
	(min)	(feet)	(ft/ft)	(ft/sec)		Sheet Flow, AB Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC
	(min) 8.3 0.4	(feet) 50 60	(ft/ft) 0.0070 0.0200	(ft/sec) 0.10 2.28		Sheet Flow, AB Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC Unpaved Kv= 16.1 fps
_	(min) 8.3	(feet) 50	(ft/ft) 0.0070	(ft/sec) 0.10		Sheet Flow, AB Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC

8.9 178 Total

Subcatchment 1: Westerly Portion of Site Including 65 Narragansett



Summary for Subcatchment 2: Majority of Site to Salt Marsh

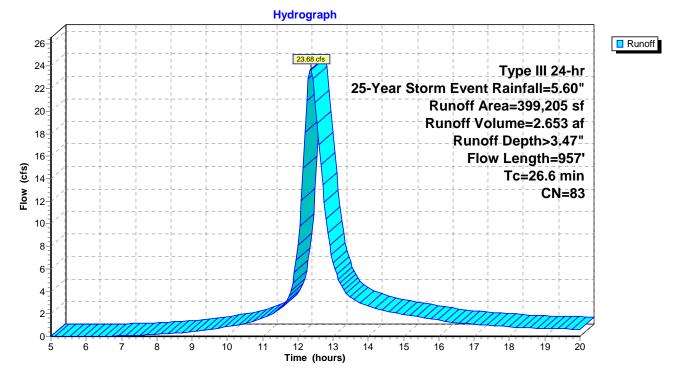
Runoff = 23.68 cfs @ 12.36 hrs, Volume= 2.653 af, Depth> 3.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Storm Event Rainfall=5.60"

_	A	rea (sf)	CN E	Description		
	3	24,786	79 V	Voods, Fai	r, HSG D	
_	74,419 98		98 V	Vater Surfa	ace, HSG D)
	399,205		83 V	Veighted A	verage	
		24,786	-		vious Area	
		74,419	1	8.64% Imp	pervious Ar	ea
	Та	Longth	Clana	Valaaitu	Conosity	Description
	Tc (min)	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	11.5	50	0.0221	0.07		Sheet Flow, AB
						Woods: Light underbrush n= 0.400 P2= 3.40"
	2.4	199	0.0755	1.37		Shallow Concentrated Flow, BC
		005	0.0400	0.00		Woodland Kv= 5.0 fps
	8.6	325	0.0160	0.63		Shallow Concentrated Flow, CD
	4.4	000	0.0007	4 55		Woodland Kv= 5.0 fps
	4.1	383	0.0967	1.55		Shallow Concentrated Flow, DE
_		0.57	T ()			Woodland Kv= 5.0 fps

26.6 957 Total

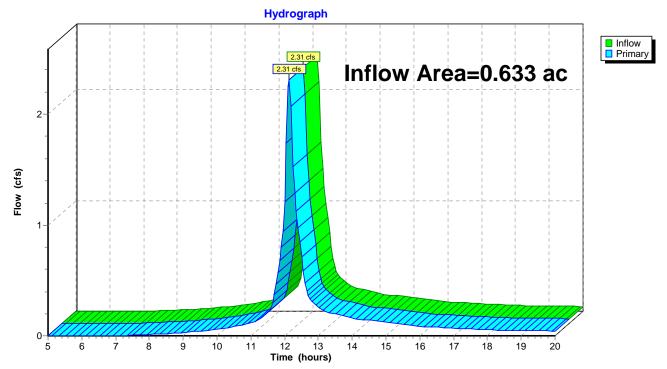
Subcatchment 2: Majority of Site to Salt Marsh



Summary for Pond 1P: Narragansett Ave Street Drains

Inflow Are	a =	0.633 ac,	6.42% Impervious, Inflow D	epth > 3.30"	for 25-Year Storm Event event
Inflow	=	2.31 cfs @	12.13 hrs, Volume=	0.174 af	
Primary	=	2.31 cfs @	12.13 hrs, Volume=	0.174 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



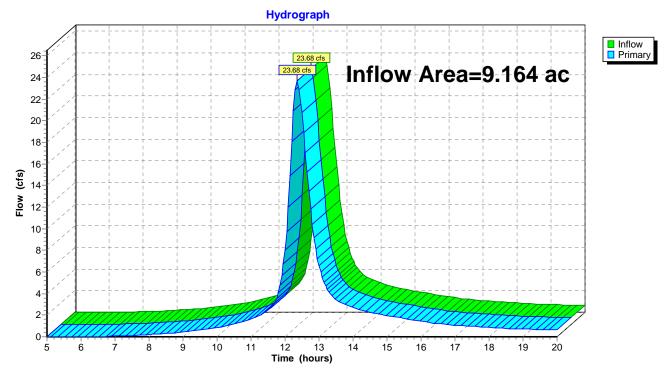
Pond 1P: Narragansett Ave Street Drains

Existing Conditions Drainage CalculationsType III 24-hr25-Year Storm Event Rainfall=5.60"Prepared by {enter your company name here}Printed 3/9/2022HydroCAD® 10.00-22s/n 07502© 2018 HydroCAD Software Solutions LLCPage 13

Summary for Pond 2P: Salt Marsh

Inflow Are	a =	9.164 ac, 18.64% Impervious, Inflow Depth > 3.47" for 25-Year Storm Event event
Inflow	=	23.68 cfs @ 12.36 hrs, Volume= 2.653 af
Primary	=	23.68 cfs @ 12.36 hrs, Volume= 2.653 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Pond 2P: Salt Marsh

Summary for Subcatchment 1: Westerly Portion of Site Including 65 Narragansett

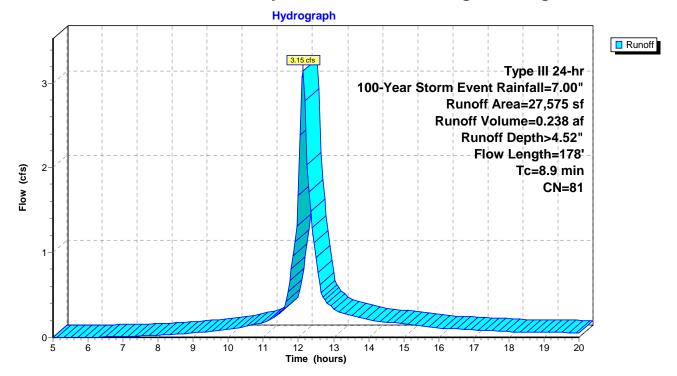
Runoff = 3.15 cfs @ 12.12 hrs, Volume= 0.238 af, Depth> 4.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Storm Event Rainfall=7.00"

_	A	rea (sf)	CN [Description		
*		1,382	98 F	Roofs/Deck	s, HSG D	
*		389	98 E	Driveway, H	ISG D	
		7,946	80 >	75% Gras	s cover, Go	ood, HSG D
_		17,858	79 V	Voods, Fai	ir, HSG D	
		27,575		Veighted A	0	
		25,804	-		rvious Area	
		1,771	771 6.42% Impervious Are			а
	Та	Longth	Clana	Volocity	Consoitu	Description
	Tc (min)	Length	Slope		Capacity	Description
_			(f+/f+)	(ft/coc)	(cfc)	
		(feet)	(ft/ft)	(ft/sec)	(cfs)	Cheet Flow AD
	8.3	(feet) 50	(ft/ft) 0.0070	(ft/sec) 0.10	(cfs)	Sheet Flow, AB
	8.3	50	0.0070	0.10	(cfs)	Grass: Short n= 0.150 P2= 3.40"
		· /			(cfs)	Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC
	8.3 0.4	50 60	0.0070 0.0200	0.10 2.28	(cfs)	Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC Unpaved Kv= 16.1 fps
	8.3	50	0.0070	0.10	(cfs)	Grass: Short n= 0.150 P2= 3.40" Shallow Concentrated Flow, BC

8.9 178 Total

Subcatchment 1: Westerly Portion of Site Including 65 Narragansett



Summary for Subcatchment 2: Majority of Site to Salt Marsh

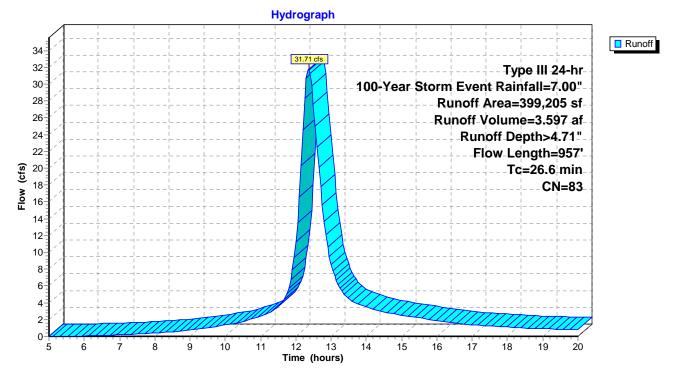
Runoff = 31.71 cfs @ 12.36 hrs, Volume= 3.597 af, Depth> 4.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Storm Event Rainfall=7.00"

A	rea (sf)	CN E	Description		
3	24,786	79 V	Voods, Fai	r, HSG D	
	74,419	98 V	Vater Surfa	ace, HSG D	
3	99,205	83 V	Veighted A	verage	
3	24,786	8	1.36% Per	vious Area	
	74,419	1	8.64% Imp	pervious Ar	ea
-				o ''	
	•	•			Description
	(feet)	(11/11)		(CIS)	
11.5	50	0.0221	0.07		Sheet Flow, AB
					Woods: Light underbrush n= 0.400 P2= 3.40"
2.4	199	0.0755	1.37		Shallow Concentrated Flow, BC
		/			Woodland Kv= 5.0 fps
8.6	325	0.0160	0.63		Shallow Concentrated Flow, CD
	000	0.0007	4 55		Woodland Kv= 5.0 fps
4.1	383	0.0967	1.55		Shallow Concentrated Flow, DE
					Woodland Kv= 5.0 fps
	3	(min) (feet) 11.5 50 2.4 199 8.6 325 4.1 383	324,786 79 V 74,419 98 V 399,205 83 V 324,786 8 74,419 1 324,786 8 74,419 1 Tc Length Slope (min) (feet) (ft/ft) 11.5 50 0.0221 2.4 199 0.0755 8.6 325 0.0160 4.1 383 0.0967	324,786 79 Woods, Fai 74,419 98 Water Surfa 399,205 83 Weighted A 324,786 81.36% Per 74,419 18.64% Imp 74,419 18.64% Imp Tc Length Slope Velocity (min) (feet) 11.5 50 2.4 199 0.0755 1.37 8.6 325 4.1 383 0.0967 1.55	324,786 79 Woods, Fair, HSG D 74,419 98 Water Surface, HSG D 399,205 83 Weighted Average 324,786 81.36% Pervious Area 324,786 81.36% Pervious Area 74,419 18.64% Impervious Area 11.5 50 0.0221 0.07 2.4 199 0.0755 1.37 8.6 325 0.0160 0.63 4.1 383 0.0967 1.55

26.6 957 Total

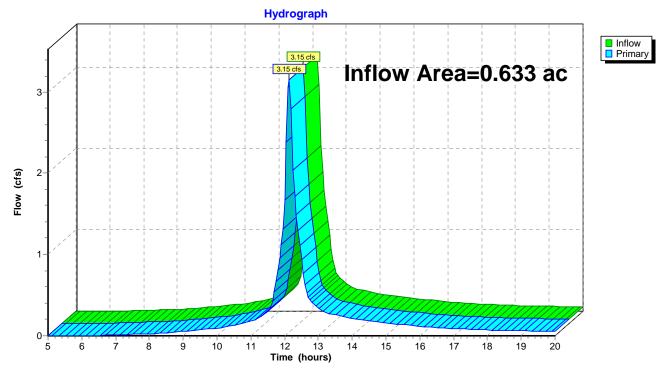
Subcatchment 2: Majority of Site to Salt Marsh



Summary for Pond 1P: Narragansett Ave Street Drains

Inflow Area =		0.633 ac,	6.42% Impervious, Inflow D	epth > 4.52"	for 100-Year Storm Event event
Inflow	=	3.15 cfs @	12.12 hrs, Volume=	0.238 af	
Primary	=	3.15 cfs @	12.12 hrs, Volume=	0.238 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

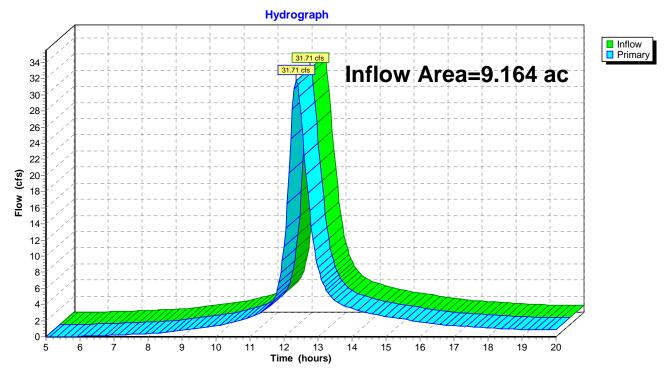


Pond 1P: Narragansett Ave Street Drains

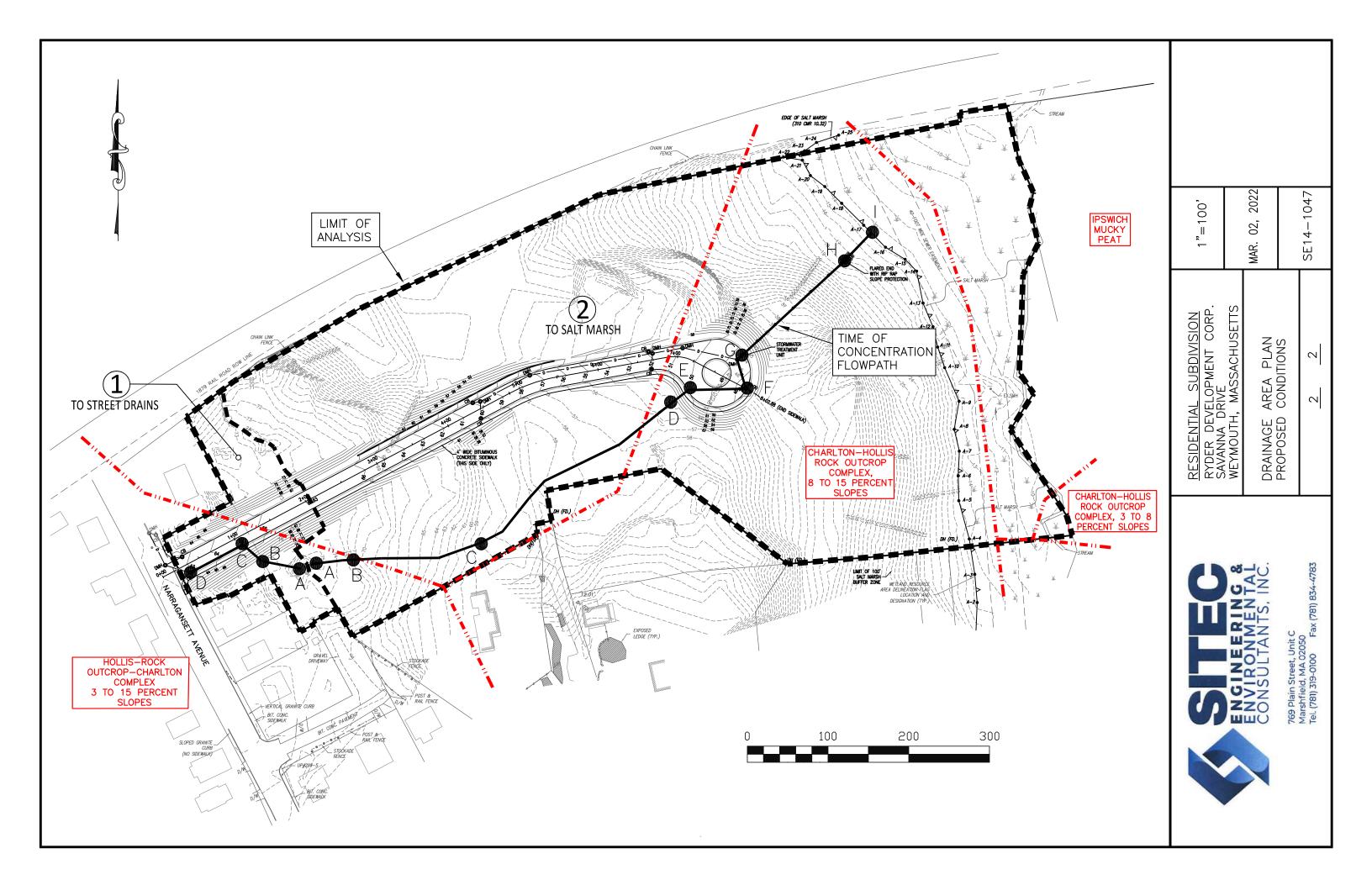
Summary for Pond 2P: Salt Marsh

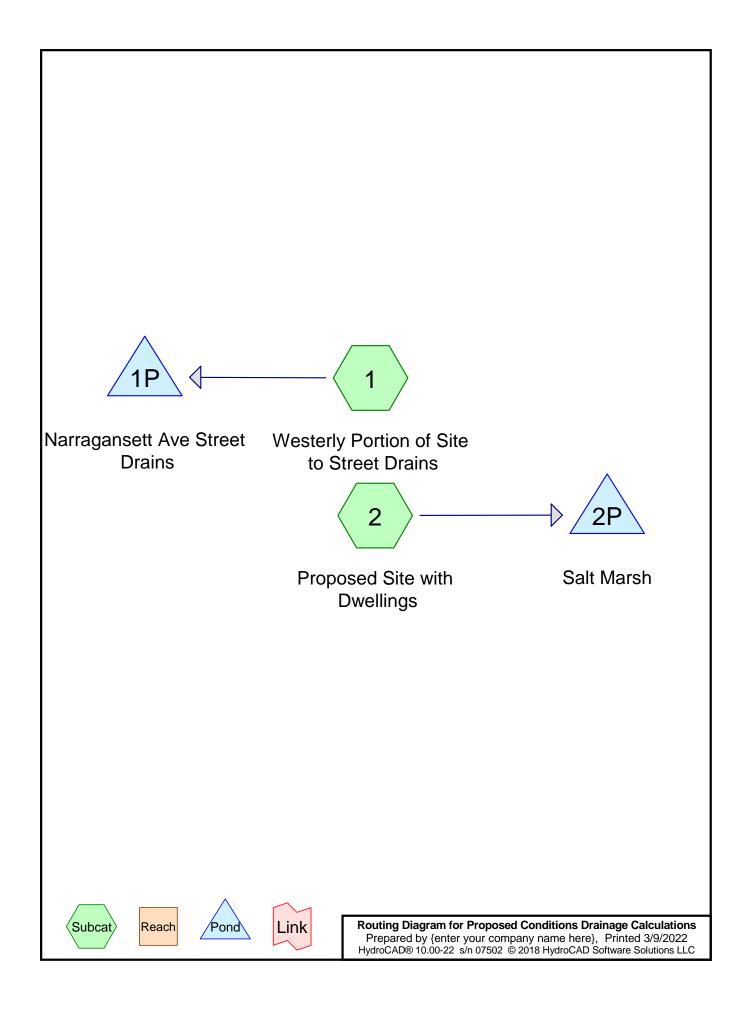
Inflow Are	a =	9.164 ac, 18.64% Impervious, Inflow Depth > 4.71" for 100-Year Storm Event event
Inflow	=	31.71 cfs @ 12.36 hrs, Volume= 3.597 af
Primary	=	31.71 cfs @ 12.36 hrs, Volume= 3.597 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Pond 2P: Salt Marsh





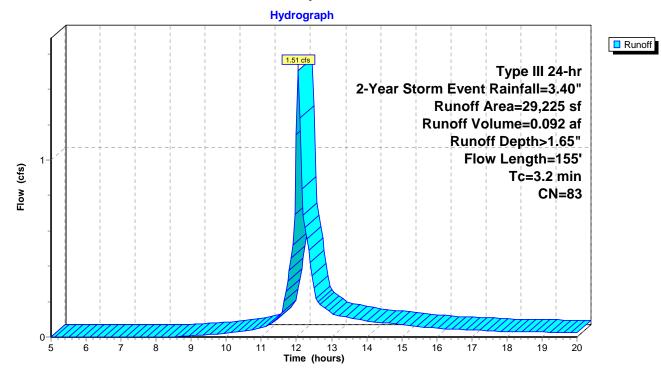
Summary for Subcatchment 1: Westerly Portion of Site to Street Drains

Runoff = 1.51 cfs @ 12.05 hrs, Volume= 0.092 af, Depth> 1.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Storm Event Rainfall=3.40"

_	A	rea (sf)	CN [Description			
	5,549 98 Paved roads w/curbs & sewers, HSG D						
_		23,676	80 >	>75% Gras	s cover, Go	bod, HSG D	
		29,225	83 \	Veighted A	verage		
		23,676	8	81.01% Per	vious Area		
		5,549		18.99% Imp	pervious Ar	ea	
	-				0		
	Tc	Length	Slope	•	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	2.7	50	0.1200	0.31		Sheet Flow, AB	
						Grass: Short n= 0.150 P2= 3.40"	
	0.1	31	0.2289	7.70		Shallow Concentrated Flow, BC	
						Unpaved Kv= 16.1 fps	
	0.4	74	0.0271	3.34		Shallow Concentrated Flow, CD	
_						Paved Kv= 20.3 fps	
	3.2	155	Total				

Subcatchment 1: Westerly Portion of Site to Street Drains

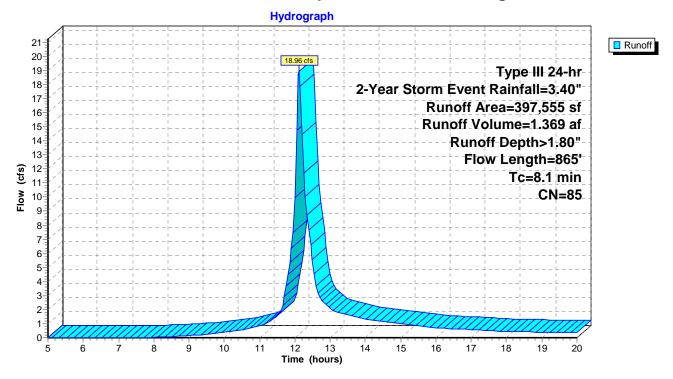


Summary for Subcatchment 2: Proposed Site with Dwellings

Runoff = 18.96 cfs @ 12.12 hrs, Volume= 1.369 af, Depth> 1.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Storm Event Rainfall=3.40"

A	Area (sf)	CN D	escription				
	20,678 98 Paved roads w/curbs & sewers, HSG D						
	200,459 80 >75% Grass cover, Good, HSG D						
	81,999	79 V	Voods, Fai	r, HSG D			
*	20,000	98 R	oofs & Dri	veways, HS	SG D		
	74,419	98 V	Vater Surfa	ace, HSG D			
:	397,555	85 V	Veighted A	verage			
	282,458	7	1.05% Per	vious Area			
	115,097	2	8.95% Imp	pervious Ar	ea		
Тс	0	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
3.1	50	0.0800	0.27		Sheet Flow, AB		
					Grass: Short n= 0.150 P2= 3.40"		
0.6	161	0.0869	4.75		Shallow Concentrated Flow, BC		
					Unpaved Kv= 16.1 fps		
3.1	297	0.0101	1.62		Shallow Concentrated Flow, CD		
0.4	07	0 4 0 0 0	0.00		Unpaved Kv= 16.1 fps		
0.1	27	0.1882	6.98		Shallow Concentrated Flow, DE		
0.0	74	0 0000	0.44		Unpaved Kv= 16.1 fps		
0.3	71	0.0282	3.41		Shallow Concentrated Flow, EF		
0.1	40	0.0200	6.42	5.04	Paved Kv= 20.3 fps Pipe Channel, FG		
0.1	40	0.0200	0.42	5.04	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'		
					n= 0.013		
0.2	170	0.1400	16.97	13.33			
0.2	170	0.1400	10.07	10.00	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'		
					n= 0.013 Concrete pipe, straight & clean		
0.6	49	0.0815	1.43		Shallow Concentrated Flow, HI		
0.0		3.00.0			Woodland Kv= 5.0 fps		
8.1	865	Total					
8.1	865	Total					

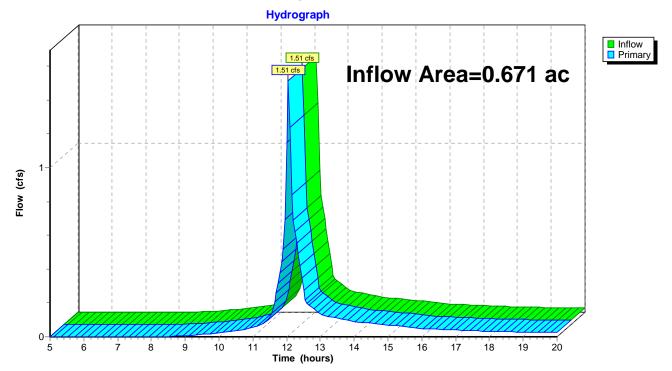


Subcatchment 2: Proposed Site with Dwellings

Summary for Pond 1P: Narragansett Ave Street Drains

Inflow Area	a =	0.671 ac, 18.99% Impervious, Inflow Depth > 1.65" for 2-Year Storm Event event	
Inflow	=	1.51 cfs @ 12.05 hrs, Volume= 0.092 af	
Primary	=	1.51 cfs @ 12.05 hrs, Volume= 0.092 af, Atten= 0%, Lag= 0.0 min	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

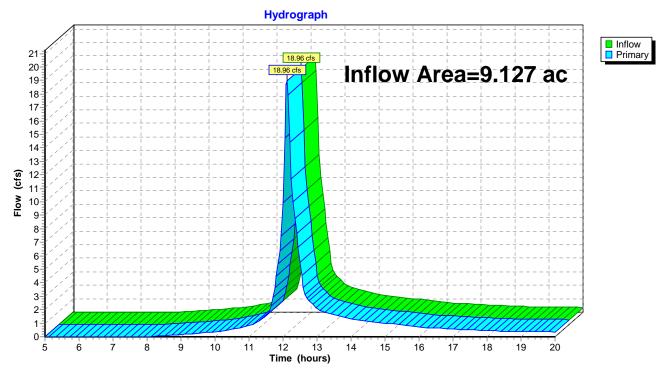


Pond 1P: Narragansett Ave Street Drains

Summary for Pond 2P: Salt Marsh

Inflow Are	a =	9.127 ac, 28.95% Impervious, Inflow Depth > 1.80" for 2-Year Storm Event event	
Inflow	=	18.96 cfs @ 12.12 hrs, Volume= 1.369 af	
Primary	=	18.96 cfs @ 12.12 hrs, Volume= 1.369 af, Atten= 0%, Lag= 0.0 min	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Pond 2P: Salt Marsh

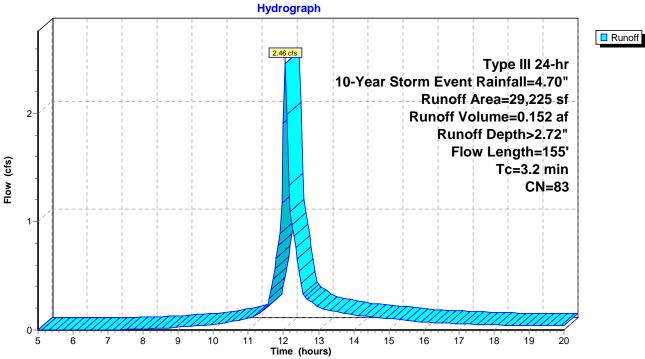
Summary for Subcatchment 1: Westerly Portion of Site to Street Drains

Runoff 2.46 cfs @ 12.05 hrs, Volume= 0.152 af, Depth> 2.72" _

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Storm Event Rainfall=4.70"

_	A	rea (sf)	CN I	Description		
	5,549 98 Paved roads w/curbs & sewers, HSG D					
_		23,676	80 >	>75% Gras	s cover, Go	bod, HSG D
		29,225	83 V	Neighted A	verage	
		23,676			vious Area	
		5,549		18.99% Imp	pervious Ar	ea
	-		<u></u>		o <i>v</i>	
	Tc	Length	Slope	•	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.7	50	0.1200	0.31		Sheet Flow, AB
						Grass: Short n= 0.150 P2= 3.40"
	0.1	31	0.2289	7.70		Shallow Concentrated Flow, BC
						Unpaved Kv= 16.1 fps
	0.4	74	0.0271	3.34		Shallow Concentrated Flow, CD
_						Paved Kv= 20.3 fps
	3.2	155	Total			

Subcatchment 1: Westerly Portion of Site to Street Drains

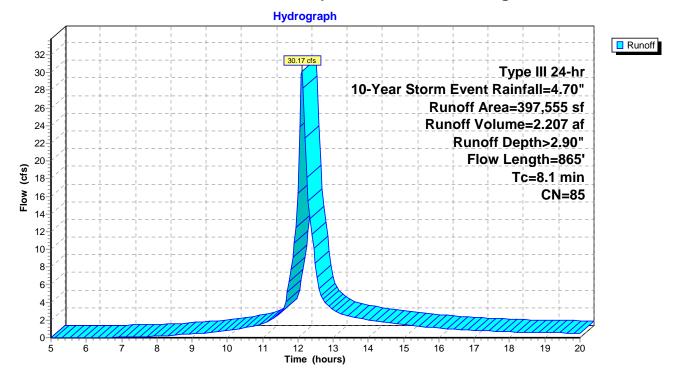


Summary for Subcatchment 2: Proposed Site with Dwellings

Runoff = 30.17 cfs @ 12.11 hrs, Volume= 2.207 af, Depth> 2.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Storm Event Rainfall=4.70"

A	Area (sf)	CN D	escription				
	20,678 98 Paved roads w/curbs & sewers, HSG D						
	200,459 80 >75% Grass cover, Good, HSG D						
	81,999	79 V	Voods, Fai	r, HSG D			
*	20,000	98 R	oofs & Dri	veways, HS	SG D		
	74,419	98 V	Vater Surfa	ace, HSG D			
:	397,555	85 V	Veighted A	verage			
	282,458	7	1.05% Per	vious Area			
	115,097	2	8.95% Imp	pervious Ar	ea		
Тс	0	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
3.1	50	0.0800	0.27		Sheet Flow, AB		
					Grass: Short n= 0.150 P2= 3.40"		
0.6	161	0.0869	4.75		Shallow Concentrated Flow, BC		
					Unpaved Kv= 16.1 fps		
3.1	297	0.0101	1.62		Shallow Concentrated Flow, CD		
0.4	07	0 4 0 0 0	0.00		Unpaved Kv= 16.1 fps		
0.1	27	0.1882	6.98		Shallow Concentrated Flow, DE		
0.0	74	0 0000	0.44		Unpaved Kv= 16.1 fps		
0.3	71	0.0282	3.41		Shallow Concentrated Flow, EF		
0.1	40	0.0200	6.42	5.04	Paved Kv= 20.3 fps Pipe Channel, FG		
0.1	40	0.0200	0.42	5.04	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'		
					n= 0.013		
0.2	170	0.1400	16.97	13.33			
0.2	170	0.1400	10.07	10.00	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'		
					n= 0.013 Concrete pipe, straight & clean		
0.6	49	0.0815	1.43		Shallow Concentrated Flow, HI		
0.0		3.00.0			Woodland Kv= 5.0 fps		
8.1	865	Total					
8.1	865	Total					

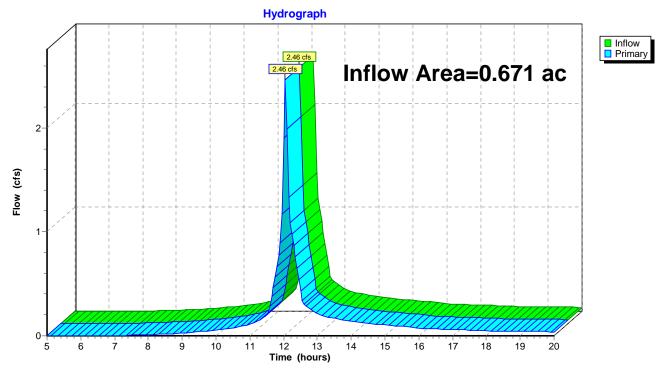


Subcatchment 2: Proposed Site with Dwellings

Summary for Pond 1P: Narragansett Ave Street Drains

Inflow Are	a =	0.671 ac, 18.99% Impervious, Inflow Depth > 2.72" for 10-Year Storm Event event
Inflow	=	2.46 cfs @ 12.05 hrs, Volume= 0.152 af
Primary	=	2.46 cfs @ 12.05 hrs, Volume= 0.152 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

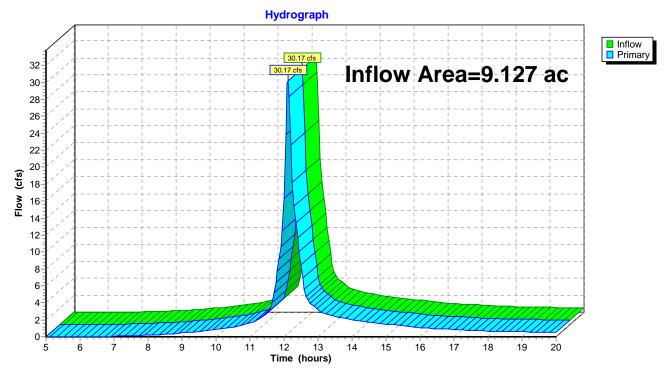


Pond 1P: Narragansett Ave Street Drains

Summary for Pond 2P: Salt Marsh

Inflow Are	a =	9.127 ac, 28.95% Impervious, Inflow Depth > 2.90" for 10-Year Storm Event event
Inflow	=	30.17 cfs @ 12.11 hrs, Volume= 2.207 af
Primary	=	30.17 cfs @ 12.11 hrs, Volume= 2.207 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Pond 2P: Salt Marsh

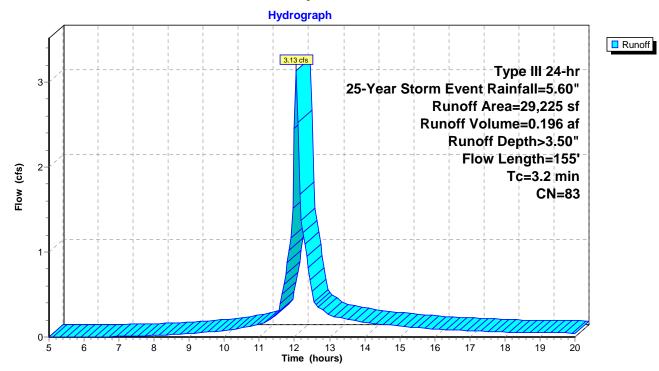
Summary for Subcatchment 1: Westerly Portion of Site to Street Drains

Runoff = 3.13 cfs @ 12.05 hrs, Volume= 0.196 af, Depth> 3.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Storm Event Rainfall=5.60"

Area (sf) CN Description										
		5,549	98	98 Paved roads w/curbs & sewers, HSG D						
_		23,676 80 >75% Grass cover, Good, HSG D								
		29,225 83 Weighted Average								
23,676 81.01% Pervious Area										
5,549 18.99% Impervious Area										
	_		-		- ·					
	Tc	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	2.7	50	0.1200	0.31		Sheet Flow, AB				
						Grass: Short n= 0.150 P2= 3.40"				
	0.1	31	0.2289	7.70		Shallow Concentrated Flow, BC				
						Unpaved Kv= 16.1 fps				
	0.4	74	0.0271	3.34		Shallow Concentrated Flow, CD				
_						Paved Kv= 20.3 fps				
	3.2	155	Total							

Subcatchment 1: Westerly Portion of Site to Street Drains

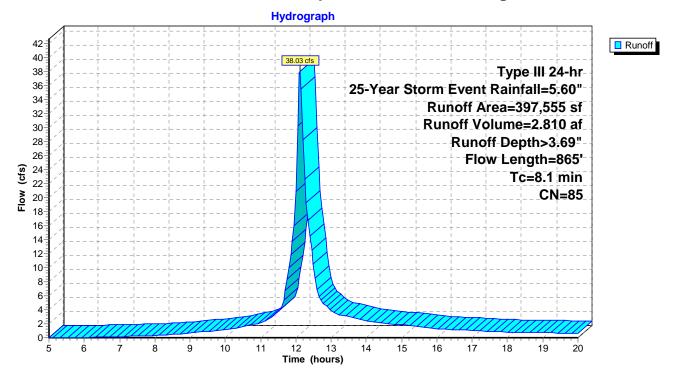


Summary for Subcatchment 2: Proposed Site with Dwellings

Runoff = 38.03 cfs @ 12.11 hrs, Volume= 2.810 af, Depth> 3.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Storm Event Rainfall=5.60"

A	Area (sf)	CN D	escription				
20,678 98 Paved roads w/curbs & sewers, HSG D							
200,459 80 >75% Grass cover, Good, HSG D							
	81,999 79 Woods, Fair, HSG D						
*	* 20,000 98 Roofs & Driveways, HSG D						
	74,419 98 Water Surface, HSG D						
	397,555 85 Weighted Average						
282,458 71.05% Pervious Area							
	115,097	2	8.95% Imp	pervious Ar	ea		
Тс	0	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
3.1	50	0.0800	0.27		Sheet Flow, AB		
					Grass: Short n= 0.150 P2= 3.40"		
0.6	161	0.0869	4.75		Shallow Concentrated Flow, BC		
					Unpaved Kv= 16.1 fps		
3.1	297	0.0101	1.62		Shallow Concentrated Flow, CD		
0.4	07	0 4 0 0 0	0.00		Unpaved Kv= 16.1 fps		
0.1	27	0.1882	6.98		Shallow Concentrated Flow, DE		
0.0	74	0 0000	0.44		Unpaved Kv= 16.1 fps		
0.3	71	0.0282	3.41		Shallow Concentrated Flow, EF		
0.1	40	0.0200	6.42	5.04	Paved Kv= 20.3 fps Pipe Channel, FG		
0.1	40	0.0200	0.42	5.04	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'		
					n= 0.013		
0.2	170	0.1400	16.97	13.33			
0.2	170	0.1400	10.07	10.00	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'		
					n= 0.013 Concrete pipe, straight & clean		
0.6	49	0.0815	1.43		Shallow Concentrated Flow, HI		
0.0		3.00.0			Woodland Kv= 5.0 fps		
8.1	865	Total					
8.1	865	Total					

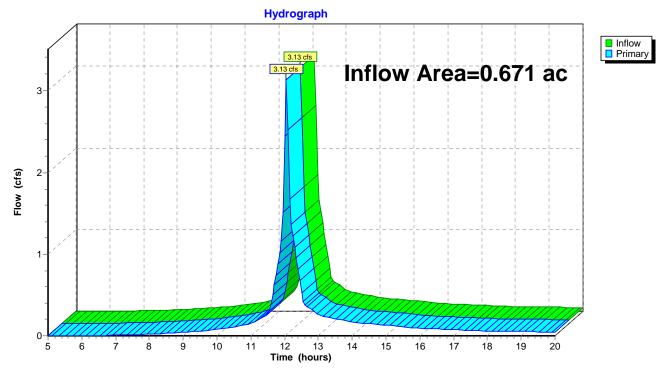


Subcatchment 2: Proposed Site with Dwellings

Summary for Pond 1P: Narragansett Ave Street Drains

Inflow Are	a =	0.671 ac, 18.99% Impervious, Inflow Depth > 3.50" for 25-Year Storm Event event
Inflow	=	3.13 cfs @ 12.05 hrs, Volume= 0.196 af
Primary	=	3.13 cfs @ 12.05 hrs, Volume= 0.196 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

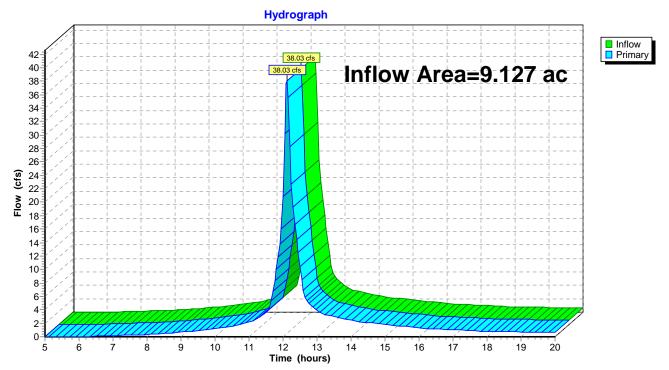


Pond 1P: Narragansett Ave Street Drains

Summary for Pond 2P: Salt Marsh

Inflow Area =		9.127 ac, 28.95% Impervious, Inflow Depth > 3.69" for 25-Year Storm Event event
Inflow	=	38.03 cfs @ 12.11 hrs, Volume= 2.810 af
Primary	=	38.03 cfs @ 12.11 hrs, Volume= 2.810 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Pond 2P: Salt Marsh

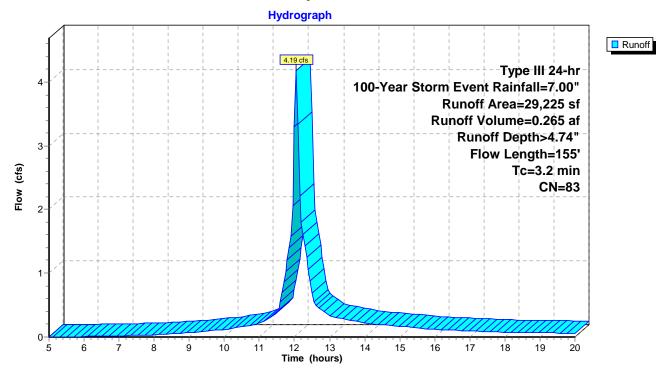
Summary for Subcatchment 1: Westerly Portion of Site to Street Drains

Runoff = 4.19 cfs @ 12.05 hrs, Volume= 0.265 af, Depth> 4.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Storm Event Rainfall=7.00"

_	A	rea (sf)	CN I	Description					
	5,549 98 Paved roads w/curbs & sewers, HSG D								
_	23,676 80 >75% Grass cover, Good, HSG D								
	29,225 83 Weighted Average								
		23,676	ł	31.01% Pei	vious Area				
		5,549		18.99% Imp	pervious Ar	ea			
	-				o 1/				
	Tc	Length	Slope		Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	2.7	50	0.1200	0.31		Sheet Flow, AB			
						Grass: Short n= 0.150 P2= 3.40"			
	0.1	31	0.2289	7.70		Shallow Concentrated Flow, BC			
						Unpaved Kv= 16.1 fps			
	0.4	74	0.0271	3.34		Shallow Concentrated Flow, CD			
_						Paved Kv= 20.3 fps			
	3.2	155	Total						

Subcatchment 1: Westerly Portion of Site to Street Drains

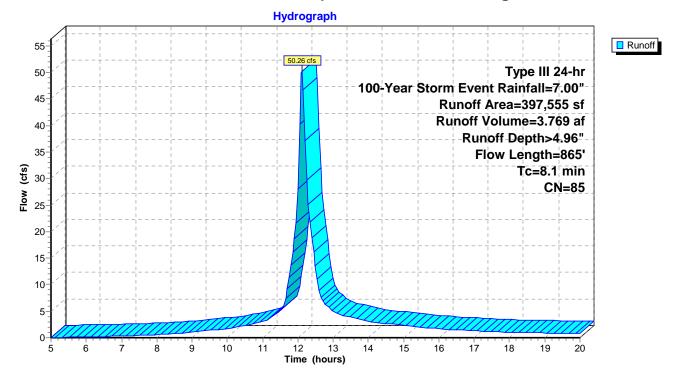


Summary for Subcatchment 2: Proposed Site with Dwellings

Runoff = 50.26 cfs @ 12.11 hrs, Volume= 3.769 af, Depth> 4.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Storm Event Rainfall=7.00"

	А	rea (sf)	CN D	escription						
_		20,678 98 Paved roads w/curbs & sewers, HSG D								
	2	00,459								
		81,999 79 Woods, Fair, HSG D								
*		20,000	98 R	oofs & Dri	veways, HS	SG D				
_		74,419	98 V	later Surfa	ace, HSG D					
	3	97,555	85 V	Veighted A	verage					
	2	82,458	7	1.05% Per	vious Area					
	1	15,097	2	8.95% Imp	pervious Ar	ea				
	Тс	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	3.1	50	0.0800	0.27		Sheet Flow, AB				
						Grass: Short n= 0.150 P2= 3.40"				
	0.6	161	0.0869	4.75		Shallow Concentrated Flow, BC				
						Unpaved Kv= 16.1 fps				
	3.1	297	0.0101	1.62		Shallow Concentrated Flow, CD				
	~ 1	07	0 4 0 0 0			Unpaved Kv= 16.1 fps				
	0.1	27	0.1882	6.98		Shallow Concentrated Flow, DE				
	0.0	74	0 0000	0.44		Unpaved Kv= 16.1 fps				
	0.3	71	0.0282	3.41		Shallow Concentrated Flow, EF				
	0.1	40	0.0200	6.42	E 04	Paved Kv= 20.3 fps				
	0.1	40	0.0200	0.42	5.04	Pipe Channel, FG 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
						n= 0.013				
	0.2	170	0.1400	16.97	13.33					
	0.2	170	0.1400	10.37	15.55	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
						n= 0.013 Concrete pipe, straight & clean				
	0.6	49	0.0815	1.43		Shallow Concentrated Flow, HI				
	0.0	40	5.0010	1.40		Woodland Kv= 5.0 fps				
_	8.1	865	Total							
	0.1	000	Total							

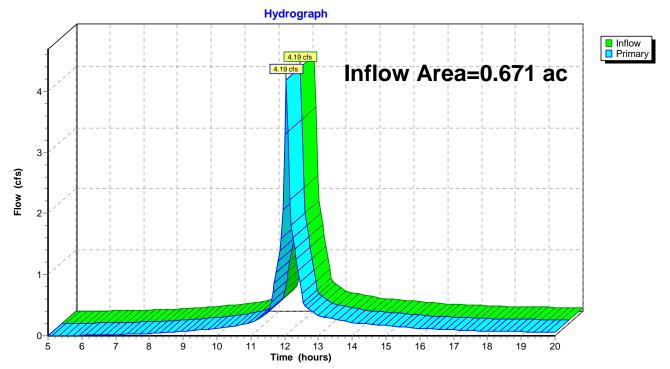


Subcatchment 2: Proposed Site with Dwellings

Summary for Pond 1P: Narragansett Ave Street Drains

Inflow Area =		0.671 ac, 18.99% Impervious, Inflow Depth > 4.74" for 100-Year Storm Event event
Inflow	=	4.19 cfs @ 12.05 hrs, Volume= 0.265 af
Primary	=	4.19 cfs @ 12.05 hrs, Volume= 0.265 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



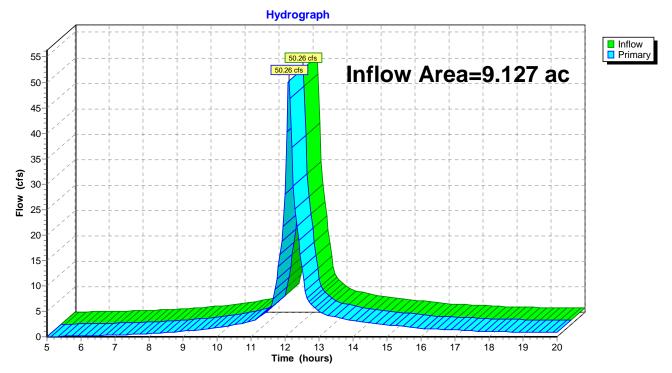
Pond 1P: Narragansett Ave Street Drains

Proposed Conditions Drainage CalculatioType III 24-hr100-Year Storm Event Rainfall=7.00"Prepared by {enter your company name here}Printed 3/9/2022HydroCAD® 10.00-22s/n 07502© 2018 HydroCAD Software Solutions LLCPage 21

Summary for Pond 2P: Salt Marsh

Inflow Are	a =	9.127 ac, 28.95% Impervious, Inflow Depth > 4.96" for 100-Year Storm Event event	
Inflow	=	50.26 cfs @ 12.11 hrs, Volume= 3.769 af	
Primary	=	50.26 cfs @ 12.11 hrs, Volume= 3.769 af, Atten= 0%, Lag= 0.0 min	

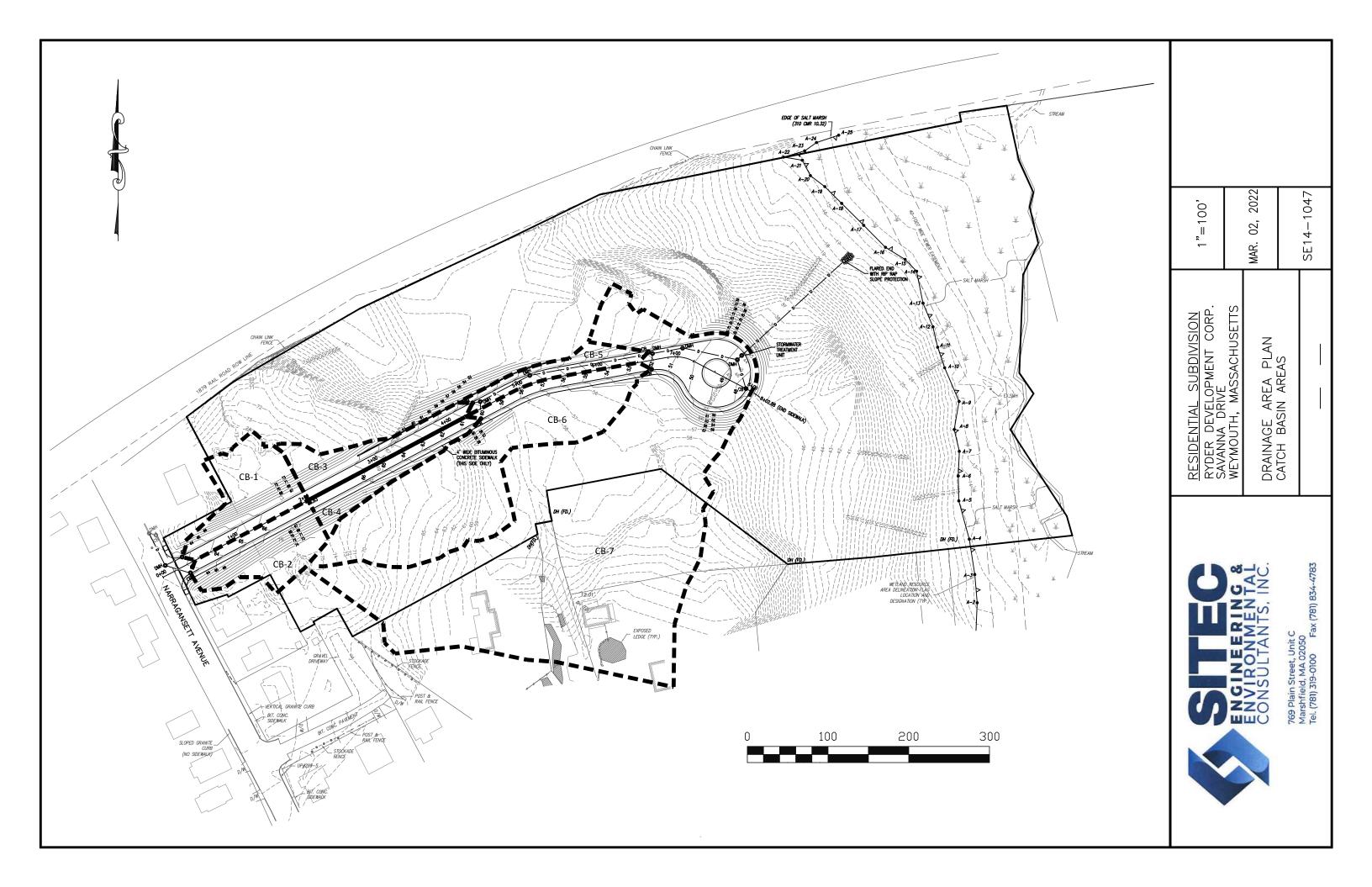
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

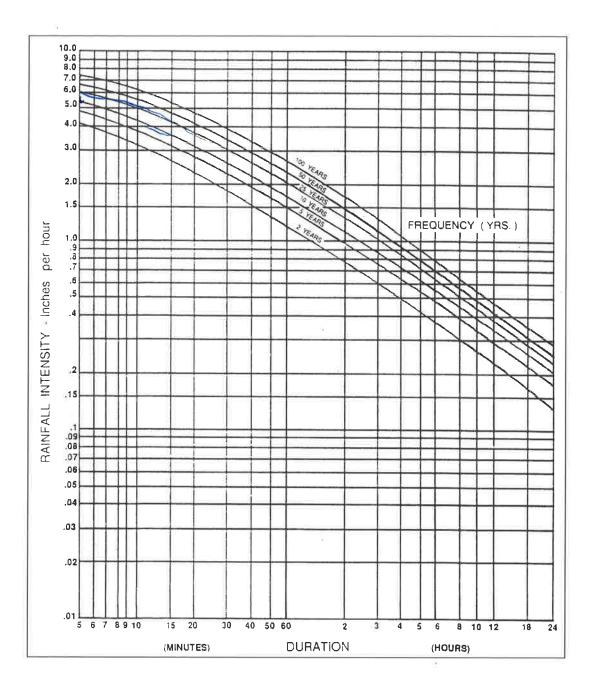


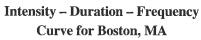
Pond 2P: Salt Marsh

SECTION 9

Storm Drain Capacity Calculations









769 Plain Street, Unit C Marshfield, MA 02050 Tel. (781) 319-0100 Fax (781) 834-4783

STORM DRAIN CAPACITY CALCULATIONS for SAVANNA DRIVE SUBDIVISION WEYMOUTH, MASSACHUSETTS March 2022

METHODOLOGY:

1)

Calculate Peak Discharges for Subcatchment Areas using Rational Method (10-Year Design Flood Frequency):

Q = C i A

where:

Q = Peak Discharge Flowrate (ft.³ / second) C = Runoff Coefficient i = Average Rainfall Intensity (in. / hr.) for a Storm Duration Equal to the Time of Concentration, T_c A = Drainage Area (acres)

2) Calculate Storm Drain Diameter Assuming Full Flow Conditions using Manning Equation:

 $D = 1.335 \left(\frac{n \ Q}{\sqrt{s}}\right)^{\frac{3}{8}}$

where:

D = Storm Drain Diameter (ft.)

- n = Manning Roughness Coefficient
- Q = Flowrate (ft. 3 / sec.)
- S = Slope of Storm Drain (ft. / ft.)

CB-1 to DMH-1:

<u>CRITERIA:</u> A = 11,595 ft.² = 0.27 acres T_c = <5 minutes

i = 5.3 in / hr. (See attached Intensity – Duration – Frequency Curve for Boston, MA)

 $C_{impervious} = 0.90$ $C_{grass} = 0.30$

$$C_{avg} = \frac{(0.05 \ acres)(0.9) + (0.22 \ acres)(0.3)}{0.27 \ acres} = 0.41$$

ANALYSIS:

$$Q = (0.41) \left(5.3 \frac{in.}{hr.} \right) (0.27 \ acres) = 0.59 \frac{ft.^3}{sec.}$$
$$D = 1.335 \left(\frac{n \ Q}{\sqrt{S}} \right)^{\frac{3}{8}} = 1.335 \left(\frac{0.013 \ (0.59)}{\sqrt{0.02}} \right)^{\frac{3}{8}} = 0.45 \ ft. = 5.4 \ inches$$

USE 12" RCP Storm Drain with S = 0.020 Maximum Capacity = 5.04 ft.³ / sec.

CB-2 to DMH-1:

CRITERIA:

 $\begin{aligned} A &= 10,164 \ \text{ft.}^2 = 0.23 \ \text{acres} \\ T_c &= <5 \ \text{minutes} \\ i &= 5.3 \ \text{in} \ / \ \text{hr.} \ \text{(See attached Intensity} - Duration - Frequency Curve for Boston, MA)} \end{aligned}$

 $C_{impervious} = 0.90$ $C_{grass} = 0.30$

$$C_{avg} = \frac{(0.07 \ acres)(0.9) + (0.16 \ acres)(0.3)}{0.23 \ acres} = 0.48$$

ANALYSIS:

$$Q = (0.48) \left(5.3 \frac{in.}{hr.} \right) (0.23 \ acres) = 0.59 \frac{ft.^3}{sec.}$$
$$D = 1.335 \left(\frac{n \ Q}{\sqrt{S}} \right)^{\frac{3}{8}} = 1.335 \left(\frac{0.013 \ (0.59)}{\sqrt{0.020}} \right)^{\frac{3}{8}} = 0.45 ft. = 5.4 \ inches$$

USE 12" RCP Storm Drain with S = 0.020Maximum Capacity = 5.04 ft.³ / sec.

DMH-1 TO EXISTING DMH IN NARRAGANSETT AVENUE Combined Flows from CB-1 and CB-2

Q = 0.59 ft.³ / sec. + 0.59 ft.³ / sec. = 1.18 ft.³ / sec. USE 12" RCP Storm Drain with S = 0.010 Maximum Capacity = 3.56 ft.³ / sec.

CB-3 to DMH-2:

CRITERIA:

 $\begin{array}{l} A=7,572 \mbox{ ft.}^2=0.17 \mbox{ acres} \\ T_{c=} \ < 5 \ \mbox{ minutes} \\ i=5.3 \mbox{ in / hr. (See attached Intensity – Duration – Frequency Curve for Boston, MA) } \end{array}$

 $C_{impervious} = 0.90$ $C_{grass} = 0.30$

$$C_{avg} = \frac{(0.08 \ acres)(0.9) + (0.09 \ acres)(0.3)}{0.17 \ acres} = 0.58$$

ANALYSIS:

$$Q = (0.58) \left(5.3 \frac{in.}{hr.} \right) (0.17 \ acres) = 0.52 \frac{ft.^3}{sec.}$$
$$D = 1.335 \left(\frac{n \ Q}{\sqrt{S}} \right)^{\frac{3}{8}} = 1.335 \left(\frac{0.013 \ (0.52)}{\sqrt{0.020}} \right)^{\frac{3}{8}} = 0.43 \ ft. = 5.1 \ inches$$

USE 12" RCP Storm Drain with S = 0.020 Maximum Capacity = 5.04 ft.³ / sec.

CB-4 to DMH-4:

CRITERIA:

A = 6,750 ft.² = 0.15 acres $T_c = < 5$ minutes i = 5.3 in / hr. (See attached Intensity – Duration – Frequency Curve for Boston, MA)

 $C_{impervious} = 0.90$ $C_{grass} = 0.30$

$$C_{avg} = \frac{(0.11 \ acres)(0.9) + (0.04 \ acres)(0.3)}{0.15 \ acres} = 0.74$$

ANALYSIS:

$$Q = (0.74) \left(5.3 \frac{in}{hr} \right) (0.15 \ acres) = 0.59 \frac{ft^3}{sec.}$$
$$D = 1.335 \left(\frac{n \ Q}{\sqrt{S}} \right)^{\frac{3}{8}} = 1.335 \left(\frac{0.013 \ (0.59)}{\sqrt{0.020}} \right)^{\frac{3}{8}} = 0.45 \ ft. = 5.4 \ inches$$

USE 12" RCP Storm Drain with S = 0.020 Maximum Capacity = 5.04 ft.³ / sec.

DMH-2 TO DMH-3 AND DMH-3 TO DMH-4 Combined Flows from CB-3 and CB-4

Q = 0.52 ft.³ / sec. + 0.59 ft.³ / sec. = 1.11 ft.³ / sec. USE 12" RCP Storm Drain with S = 0.036 Maximum Capacity = 6.76 ft.³ / sec.

<u>CB-5 to DMH-4:</u>

CRITERIA:

 $\begin{array}{l} A=5,122 \mbox{ ft.}^2=0.12 \mbox{ acres} \\ T_c\ =<5 \ \mbox{ minutes} \\ i=5.3 \mbox{ in / hr. (See attached Intensity – Duration – Frequency Curve for Boston, MA)} \end{array}$

 $C_{impervious} = 0.90$ $C_{grass} = 0.30$

$$C_{avg} = \frac{(0.08 \ acres)(0.9) + (0.04 \ acres)(0.3)}{0.12 \ acres} = 0.70$$

ANALYSIS:

$$Q = (0.70) \left(5.3 \frac{in.}{hr.} \right) (0.12 \ acres) = 0.45 \frac{ft.^3}{sec.}$$
$$D = 1.335 \left(\frac{n \ Q}{\sqrt{S}} \right)^{\frac{3}{8}} = 1.335 \left(\frac{0.013 \ (0.45)}{\sqrt{0.020}} \right)^{\frac{3}{8}} = 0.40 \ ft. = 4.9 \ inches$$

USE 12" RCP Storm Drain with S = 0.020Maximum Capacity = 5.04 ft.³ / sec.

<u>CB-6 to DMH-4:</u>

CRITERIA:

A = 37,590 ft.² = 0.86 acres T_c = 5.9 minutes i = 5.0 in / hr. (See attached Intensity – Duration – Frequency Curve for Boston, MA)

 $C_{impervious} = 0.90$ $C_{grass} = 0.30$

$$C_{avg} = \frac{(0.22 \ acres)(0.9) + (0.64 \ acres)(0.3)}{0.86 \ acres} = 0.45$$

ANALYSIS:

$$Q = (0.45) \left(5.0 \frac{in.}{hr.} \right) (0.86 \ acres) = 1.93 \frac{ft.^3}{sec.}$$
$$D = 1.335 \ \left(\frac{n \ Q}{\sqrt{S}} \right)^{\frac{3}{8}} = 1.335 \left(\frac{0.013 \ (1.93)}{\sqrt{0.020}} \right)^{\frac{3}{8}} = 0.70 \ ft. = 8.4 \ inches$$

USE 12" RCP Storm Drain with S = 0.020 Maximum Capacity = 5.04 ft.³ / sec.

DMH-4 TO DMH-5

Combined Flows from DMH-3, CB-5 and CB-6

Q = 1.11 ft.³ / sec. + 0.45 ft.³ / sec. + 1.93 ft.³ / sec = 3.49 ft.³ / sec. USE 12" RCP Storm Drain with S = 0.036 Maximum Capacity = 6.76 ft.³ / sec.

<u>DMH-5 TO DMH-6</u> Combined Flows from DMH-3, CB-5 and CB-6

Q = 1.11 ft.³ / sec. + 0.45 ft.³ / sec. + 1.93 ft.³ / sec = 3.49 ft.³ / sec. USE 12" RCP Storm Drain with S = 0.020 Maximum Capacity = 5.04 ft.³ / sec.

<u>CB-7 to DMH-6:</u>

CRITERIA:

A = 111,476 ft.² = 2.56 acres

 $T_c = 7.9$ minutes

i = 4.8 in / hr. (See attached Intensity – Duration – Frequency Curve for Boston, MA)

 $C_{impervious} = 0.90$ $C_{grass} = 0.30$ $C_{wooded} = 0.20$

$$C_{avg} = \frac{(0.47 \ acres)(0.9) + (1.84 \ acres)(0.3) + (0.25 \ acres)(0.2)}{2.56 \ acres} = 0.40$$

ANALYSIS:

$$Q = (0.40) \left(4.8 \frac{in.}{hr.}\right) (2.56 \ acres) = 4.92 \frac{ft.^3}{sec.}$$
$$D = 1.335 \left(\frac{n \ Q}{\sqrt{S}}\right)^{\frac{3}{8}} = 1.335 \left(\frac{0.013 \ (4.92)}{\sqrt{0.020}}\right)^{\frac{3}{8}} = 0.99 \ ft. = 11.90 \ inches$$

USE 15" RCP Storm Drain with S = 0.020Maximum Capacity = 9.13 ft.³ / sec.

DMH-6 to STORMWATER TREATMENT UNIT: Combined Flows CB-7 AND DMH-5

Q = 3.49 ft.³ / sec. + 4.92 ft.³ / sec. ft.³ / sec = 8.41 ft.³ / sec. USE 15" RCP Storm Drain with S = 0.020 Maximum Capacity = 9.13 ft.³ / sec.

SECTION 10 Stormwater Treatment Unit Water Quality & TSS Removal Calculations

Project: Location: Prepared For:	Savanna Drive Weymouth, MA SITEC / Jeff Couture	
Purpose:	To calculate the water quality flow rate (WQF) over a given site area. In this si	tuation the WQE is

- derived from the first 1" of runoff from the contributing impervious surface.
- Reference:
 Massachusetts Dept. of Environmental Protection Wetlands Program / United States Department of Agriculture Natural Resources Conservation Service TR-55 Manual
- **Procedure:** Determine unit peak discharge using Figure 1 or 2. Figure 2 is in tabular form so is preferred. Using the tc, read the unit peak discharge (qu) from Figure 1 or Table in Figure 2. qu is expressed in the following units: cfs/mi²/watershed inches (csm/in).

Compute Q Rate using the following equation:

Q = (qu) (A) (WQV)

where:

Q = flow rate associated with first 1" of runoff

qu = the unit peak discharge, in csm/in.

A = impervious surface drainage area (in square miles)

WQV = water quality volume in watershed inches (1" in this case)

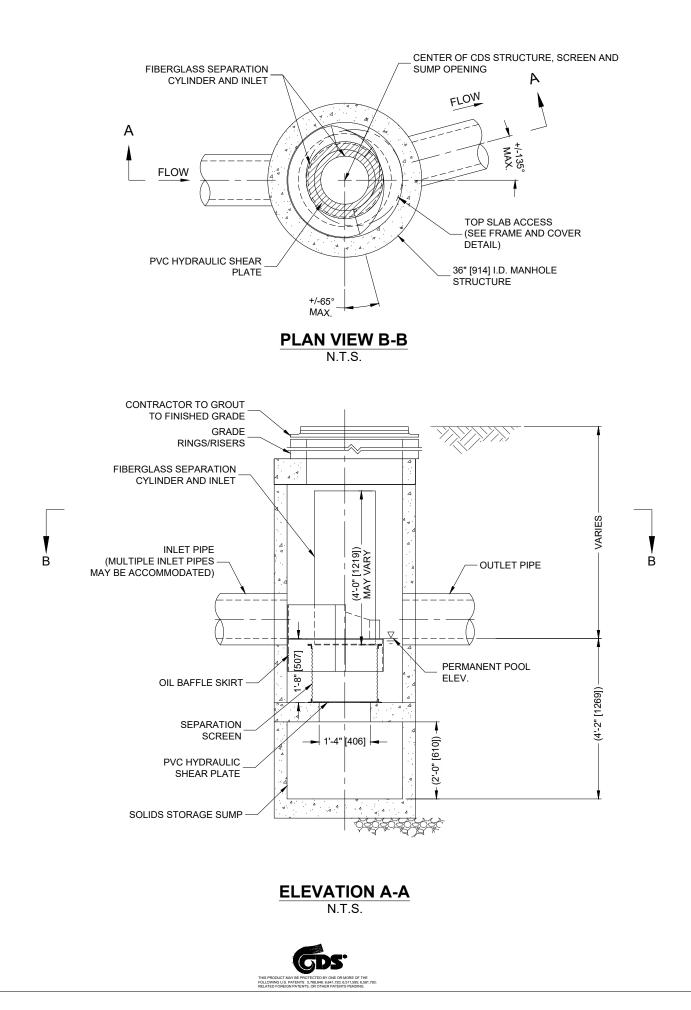
Structure Name	Impv. (acres)	A (miles ²)	t _c (min)	t _c (hr)	WQV (in)	qu (csm/in.)	Q (cfs)
STU 1	0.73	0.0011406		0.083	1.00	795.00	0.91





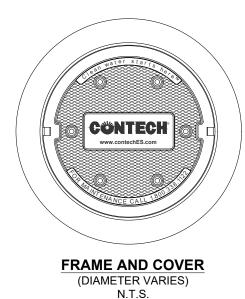
CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION **BASED ON THE RATIONAL RAINFALL METHOD** SAVANNA DRIVE WEYMOUTH, MA 0.73 ac Unit Site Designation STU 1 Area Rainfall Station # Weighted C 0.9 69 5 min t_c CDS Model 1515-3 **CDS** Treatment Capacity 1.0 cfs Rainfall Percent Rainfall Cumulative Total Flowrate **Treated Flowrate** Incremental Intensity¹ Volume¹ **Rainfall Volume** Removal (%) (cfs) (cfs) <u>(in/hr)</u> 10.2% 0.02 10.2% 0.01 0.01 10.2 0.03 0.03 9.6 0.04 9.6% 19.8% 0.06 9.4% 29.3% 0.04 0.04 9.4 37.0% 7.7% 0.05 7.6 0.08 0.05 0.10 8.6% 45.6% 0.07 0.07 8.4 0.12 6.3% 51.9% 0.08 0.08 6.1 4.7% 0.14 56.5% 0.09 0.09 4.5 0.16 4.6% 61.2% 0.11 0.11 4.5 0.18 3.5% 64.7% 0.12 0.12 3.4 0.20 4.3% 69.1% 0.13 0.13 4.1 0.25 8.0% 77.1% 0.16 0.16 7.5 0.30 0.20 5.1 5.6% 82.7% 0.20 0.35 4.4% 87.0% 0.23 0.23 3.9 0.40 2.5% 89.5% 0.26 0.26 2.3 2.2 0.45 92.1% 0.30 0.30 2.5% 0.50 1.4% 93.5% 0.33 0.33 1.2 0.75 5.0% 98.5% 0.49 0.49 3.9 0.7 1.0% 99.5% 0.66 0.66 1.00 1.50 0.0% 99.5% 0.99 0.99 0.0 2.00 0.0% 99.5% 1.31 1.00 0.0 3.00 0.5% 100.0% 1.97 1.00 0.1 95.0 Removal Efficiency Adjustment² = 6.5% Predicted % Annual Rainfall Treated = 93.3% Predicted Net Annual Load Removal Efficiency = 88.5% 1 - Based on 10 years of hourly precipitation data from NCDC Station 770, Boston WSFO AP, Suffolk County, MA 2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

CDS1515-3-C DESIGN NOTES



CDS1515-3-C RATED TREATMENT CAPACITY IS 1.0 CFS, OR PER LOCAL REGULATIONS.

THE STANDARD CDS1515-3-C CONFIGURATION IS SHOWN.



GENERAL NOTES

- 1. CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE. 2. FOR SITE SPECIFIC DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHT, PLEASE CONTACT YOUR CONTECH ENGINEERED
- SOLUTIONS LLC REPRESENTATIVE. www.ContechES.com 3. CDS WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING.
- CONTRACTOR TO CONFIRM STRUCTURE MEETS REQUIREMENTS OF PROJECT. 4. STRUCTURE SHALL MEET AASHTO HS20 LOAD RATING, ASSUMING EARTH COVER OF 0' - 2', AND GROUNDWATER ELEVATION AT, OR BELOW,
- THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION. CASTINGS SHALL MEET AASHTO M306 AND BE CAST WITH THE CONTECH LOGO.
- 5. IF REQUIRED, PVC HYDRAULIC SHEAR PLATE IS PLACED ON SHELF AT BOTTOM OF SCREEN CYLINDER. REMOVE AND REPLACE AS NECESSARY DURING MAINTENANCE CLEANING.
- 6. CDS STRUCTURE SHALL BE PRECAST CONCRETE CONFORMING TO ASTM C-478 AND AASHTO LOAD FACTOR DESIGN METHOD.

INSTALLATION NOTES

- A. ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE CDS MANHOLE STRUCTURE. CONTRACTOR TO INSTALL JOINT SEALANT BETWEEN ALL STRUCTURE SECTIONS AND ASSEMBLE STRUCTURE. C.
- CONTRACTOR TO PROVIDE, INSTALL, AND GROUT INLET AND OUTLET PIPE(S). MATCH PIPE INVERTS WITH ELEVATIONS SHOWN. ALL PIPE D.
- CENTERLINES TO MATCH PIPE OPENING CENTERLINES.
- E. CONTRACTOR TO TAKE APPROPRIATE MEASURES TO ASSURE UNIT IS WATER TIGHT, HOLDING WATER TO FLOWLINE INVERT MINIMUM. IT IS SUGGESTED THAT ALL JOINTS BELOW PIPE INVERTS ARE GROUTED.



SITE SPECIFIC DATA REQUIREMENTS

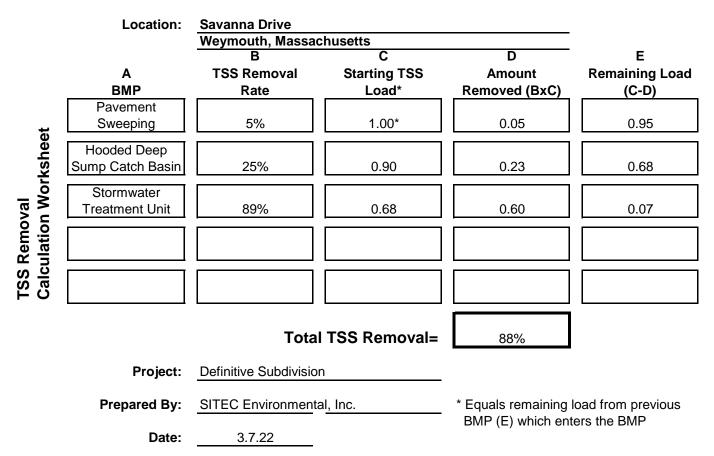
STRUCTURE ID								
WATER QUALITY	WATER QUALITY FLOW RATE (CFS OR L/s) *							
PEAK FLOW RAT	E (CFS OR I	L/s)			*			
RETURN PERIOD	OF PEAK F	LO	W (YRS)		*			
SCREEN APERTU	JRE (2400 C)R 4	700)		*			
PIPE DATA:	I.E.	N	MATERIAL	D	IAMETER			
INLET PIPE 1	*		*		*			
INLET PIPE 2	*		*		*			
OUTLET PIPE	*		*		*			
RIM ELEVATION *								
ANTI-FLOTATION	BALLAST		WIDTH		HEIGHT			
* *								
NOTES/SPECIAL REQUIREMENTS:								
* PER ENGINEER	* PER ENGINEER OF RECORD							

CDS1515-3-C

ONLINE CDS

STANDARD DETAIL

SECTION 11 Total Suspended Solids Removal Calculation Worksheet



Total Suspended Solid Removal Calculation Worksheet 1 of 1

SECTION 12

Stormwater Management System Operation & Maintenance Plan



Stormwater Management System OPERATION AND MAINTENANCE PLAN March 2022

SAVANNA DRIVE SUBDIVISION Weymouth, MA

An important element of the overall stormwater management system is the regular maintenance of the control components. Specifically, the effectiveness of the sediment control components is dependent upon their continued maintenance and repair. These structures are particularly important in locations where upgradient areas are not fully stabilized and may be subject to erosion. As natural deterioration of these barriers occurs, replacement and/or repair efforts must be coordinated by removing the accumulated sediment and extending the barrier laterally, as required.

Extreme weather conditions can serve to highlight the need for a vigorous maintenance program as well as a need to fine-tune and improve upon the system's design. The following section outlines a recommended plan for long term maintenance and immediate repair and improvement of the sediment controls.

The performance of the proposed maintenance program shall include the following responsibilities and authorities:

During Construction

The erosion control barrier consisting of silt socks filled with compost installed along the down-gradient side of all construction shall be inspected frequently by the contractor. Should there be indications of damage or deterioration of these devices, they shall be removed and replaced immediately.

Supplemental silt socks or haybale check dams shall be placed around installed catch basins. These will discourage the transmission of sediments into stormwater controls while vegetation is being established. Any accumulated sediments within these controls shall be removed.

In order for the contractor to respond to the performance requirements outlined above, the contractor shall be required to maintain an ample supply of silt socks or haybales for emergency stabilization and repair work. The implementation of the recommended repair work and maintenance program will improve the long-term effectiveness of the stormwater control structures.



Routine System Maintenance

After the completion of construction, the roadways and stormwater management system shall be inspected and maintained by the applicant until the Town accepts responsibility for the roadways. Bi-annual inspections shall be conducted on the catch basins, drainage manholes and stormwater treatment unit. Accumulated sediment shall be removed from the catch basins in accordance with Weymouth Department of Public Works biannual maintenance schedule, if accumulated sediment meets or exceeds a sump depth of 2-feet, or if accumulated sediment affects the performance of the stormwater treatment unit in accordance with the manufacturer's guidelines. Disposal of the accumulated sediment must be in accordance with applicable local, state and federal guidelines and regulations.

Sweeping of the pavement shall be conducted in accordance with Weymouth Department of Public Works biannual maintenance schedule, unless more frequent sweeping is required. This will further limit sediment accumulation in the stormwater control structures.